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Sanyal et al.

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(54) **DEPTH RESOLVED NONINVASIVE
GLUCOSE CONCENTRATION
DETERMINATION ANALYZER APPARATUS
AND METHOD OF USE THEREOF**

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filed on Dec. 2, 2017, now abandoned, which is a
(Continued)

(51) **Int. Cl.**
A61B 5/1455 (2006.01)
A61B 5/145 (2006.01)
(Continued)

(52) **U.S. Cl.**
CPC **A61B 5/14532** (2013.01); **A61B 5/0075**
(2013.01); **A61B 5/1455** (2013.01); **A61B**
5/6832 (2013.01); **G01J 2003/106** (2013.01)

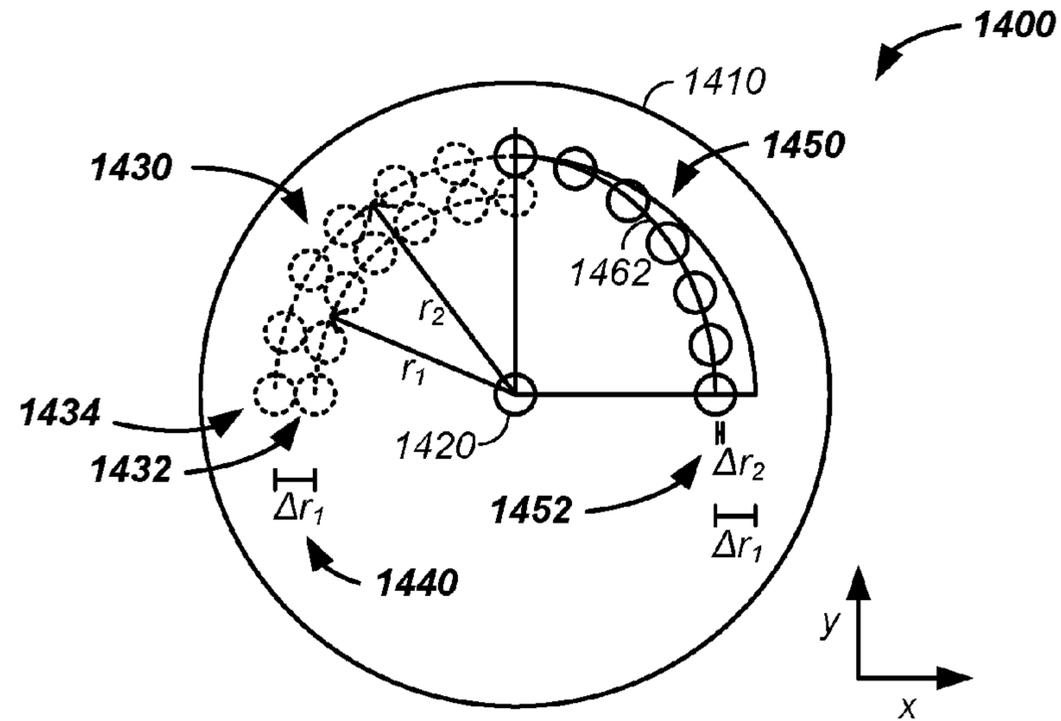
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CPC **A61B 5/1455**; **A61B 5/14551**; **A61B**
5/14552; **A61B 5/14532**; **A61B 5/6832**;
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See application file for complete search history.

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(57) **ABSTRACT**
The invention comprises a method for noninvasively deter-
mining a sample property, comprising controlling photon
generation from a source and analyzing signal from a set of
detectors; irradiating an illumination zone of skin with the
photons; and detecting diffusely reflected photons from the
skin, the set of detectors respectively optically coupled to a
set of detection zones of the skin positioned along a spiral
path between a first and second radial distance from the
illumination zone, where a first detection zone of a first
detector of the set of detectors extends radially outward
from the illumination zone to at least an inward radial
distance, from the illumination zone, of a second detection
zone of a second detector of the set of detectors, where
at least one detection zone of the set of detection zones
has a central radial distance from the illumination zone
between the first and second radial distances.

6 Claims, 11 Drawing Sheets



Related U.S. Application Data

continuation-in-part of application No. 15/636,073,
filed on Jun. 28, 2017, now abandoned.

(60) Provisional application No. 62/355,507, filed on Jun.
28, 2016.

(51) **Int. Cl.**
A61B 5/00 (2006.01)
G01J 3/10 (2006.01)

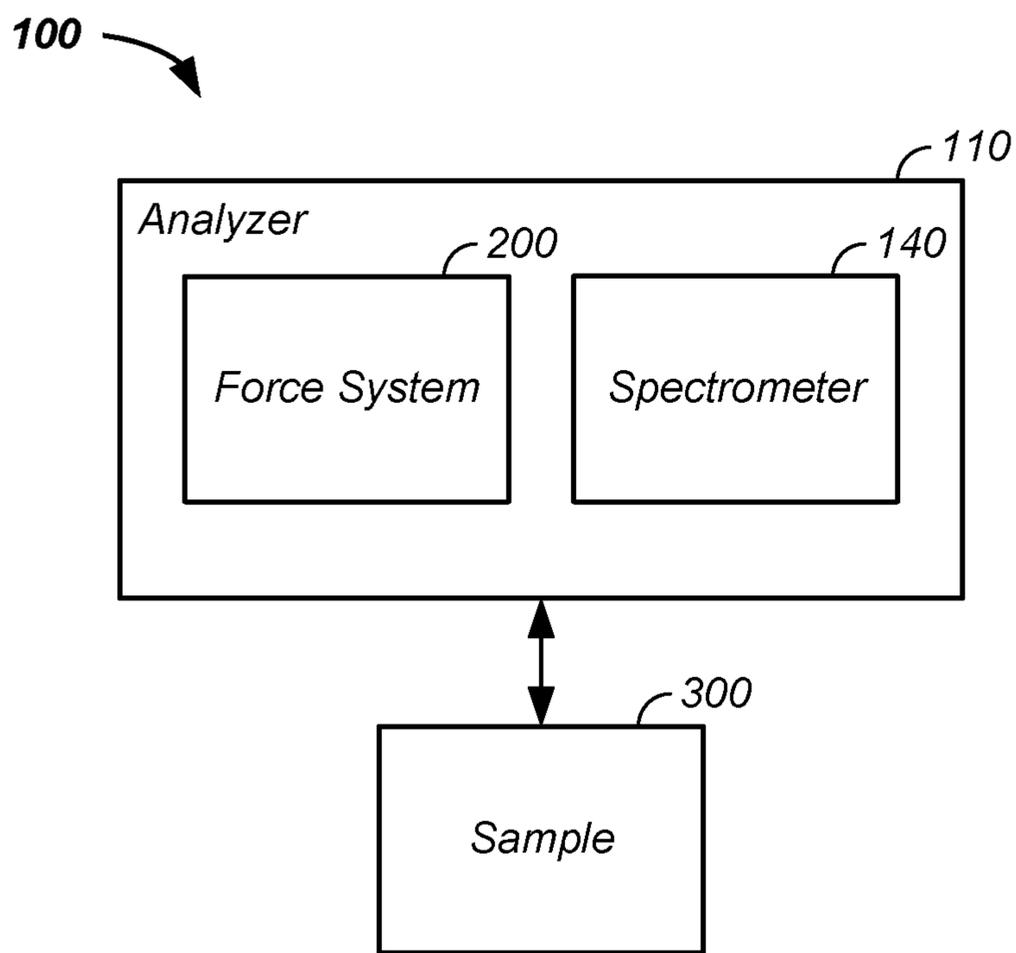


FIG. 1

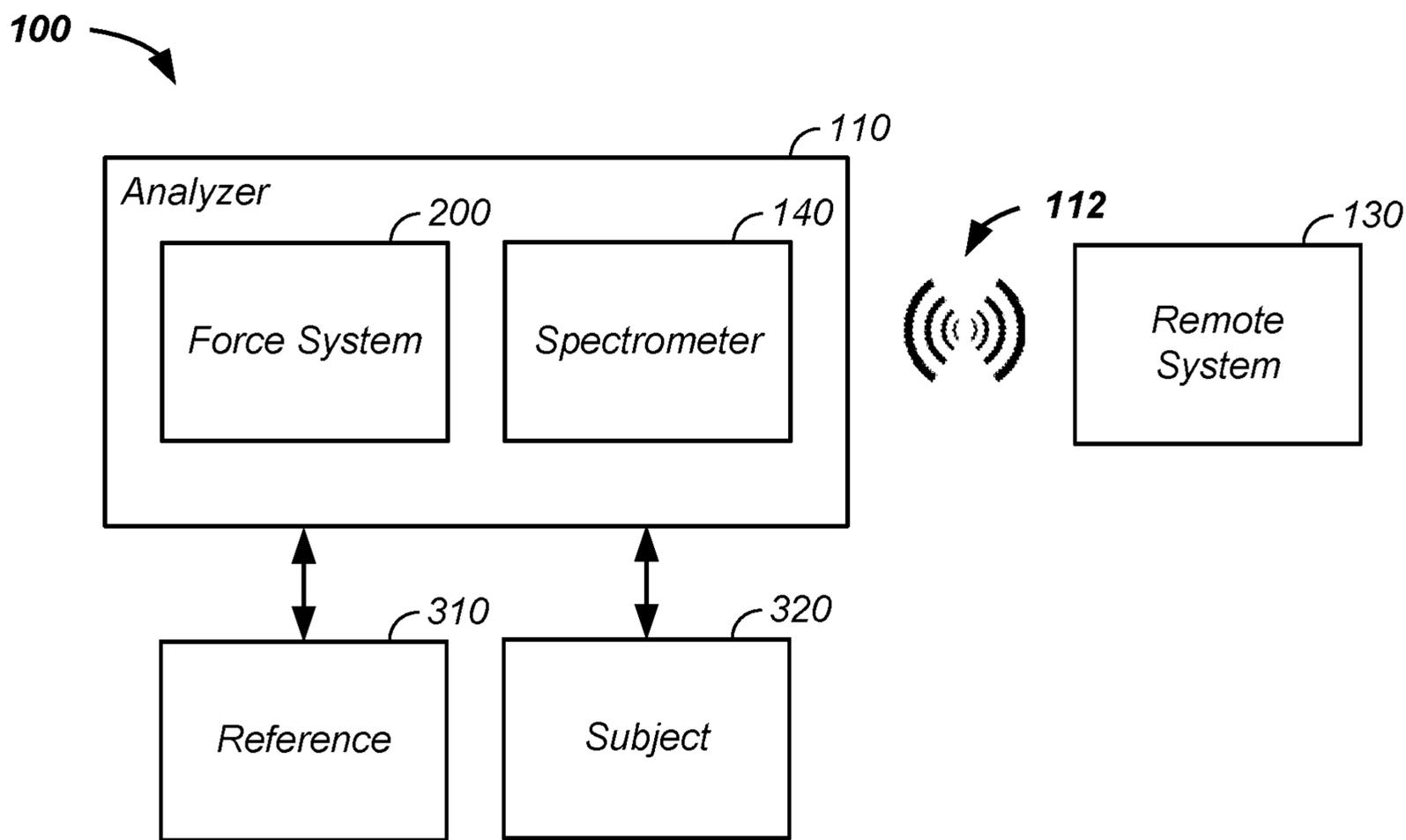


FIG. 2

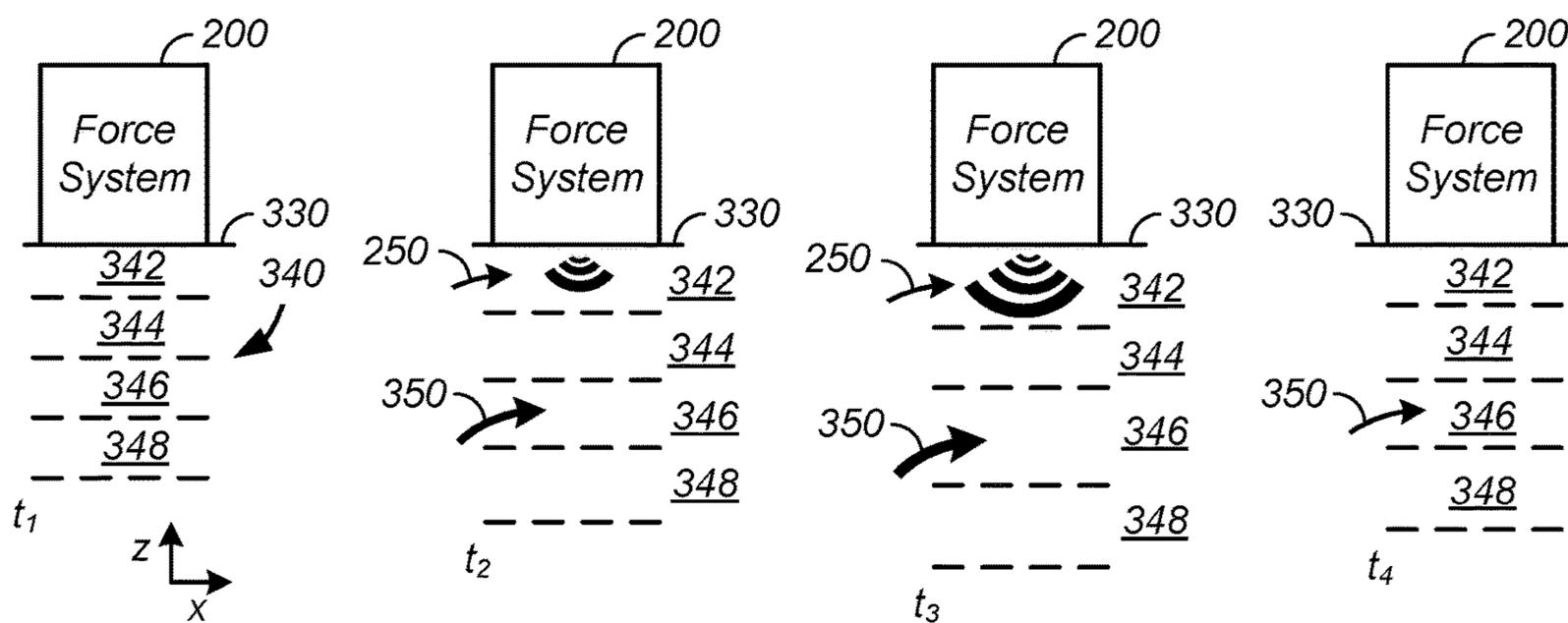


FIG. 3A

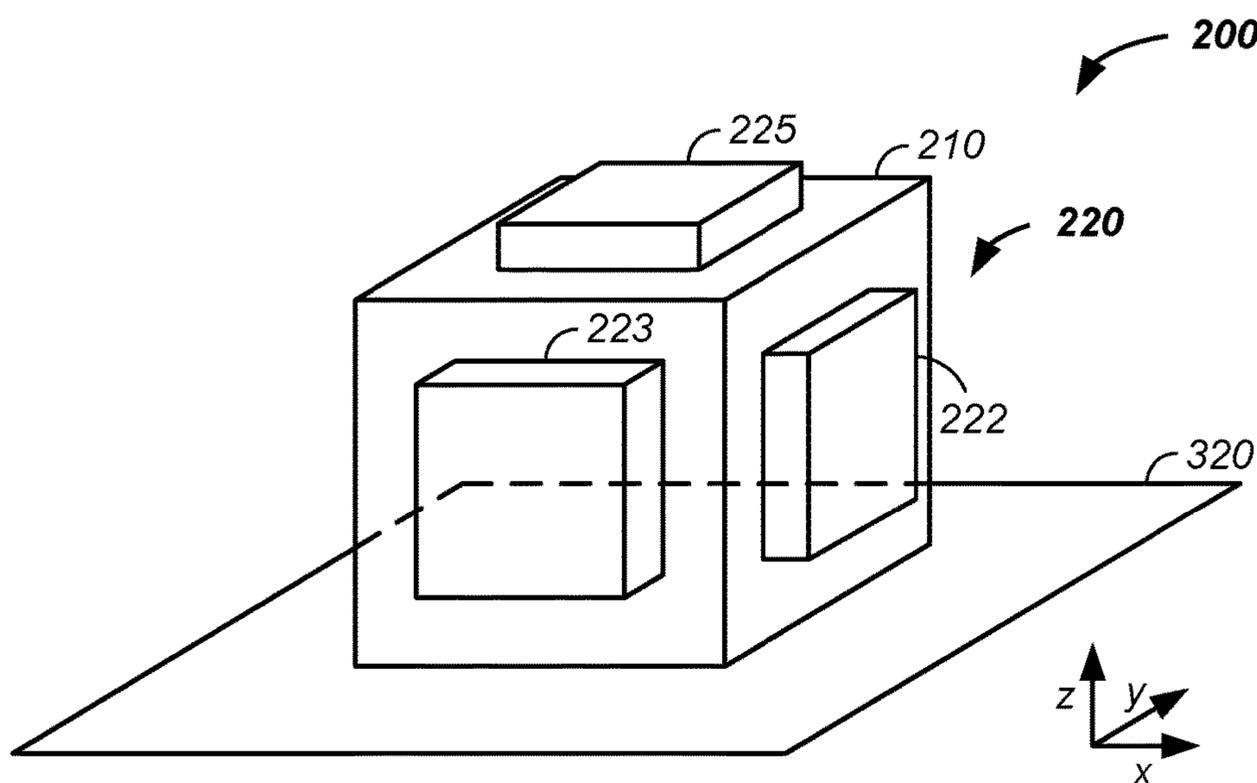


FIG. 3B

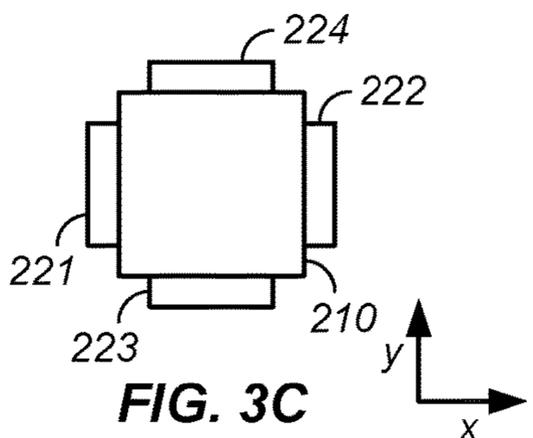


FIG. 3C

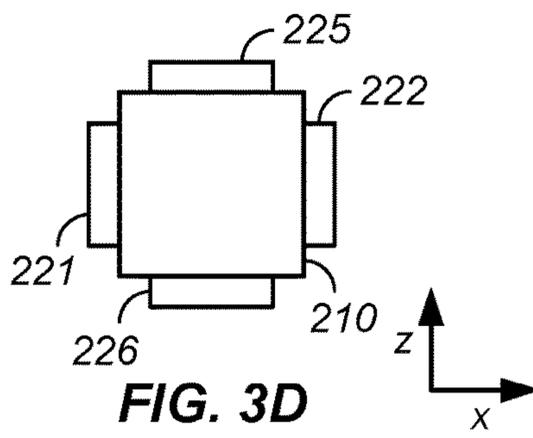


FIG. 3D

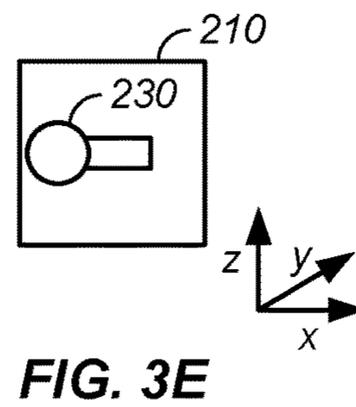


FIG. 3E

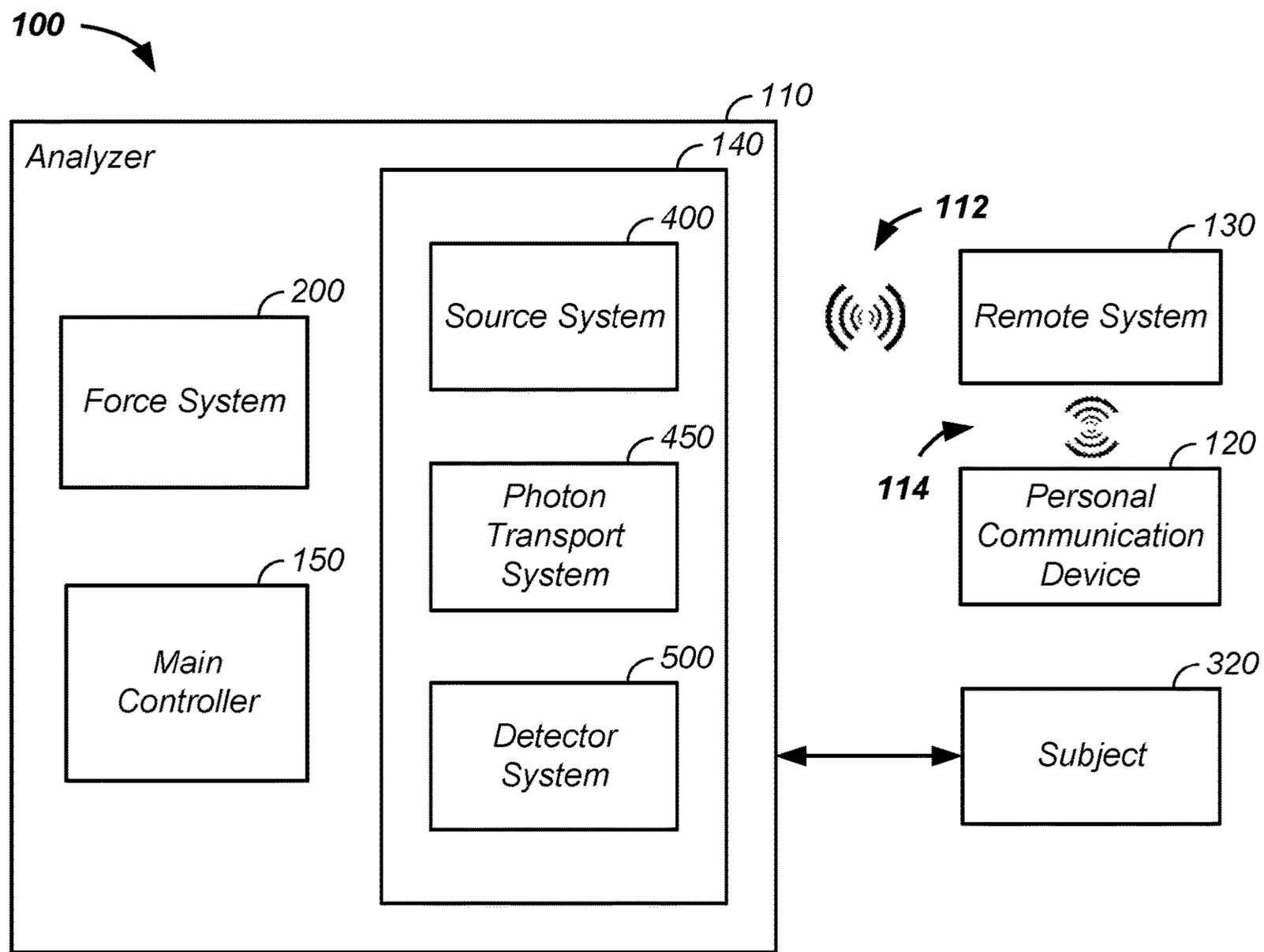


FIG. 4A

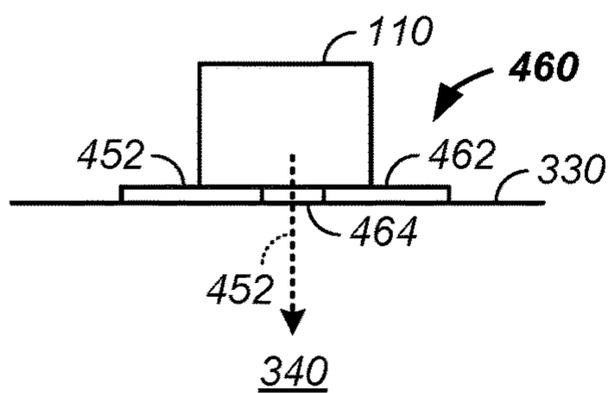


FIG. 4B

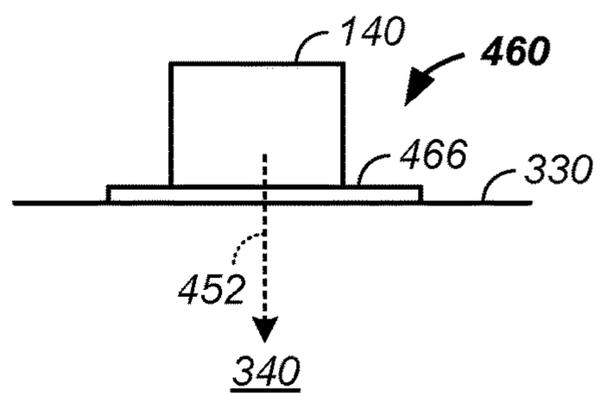


FIG. 4C

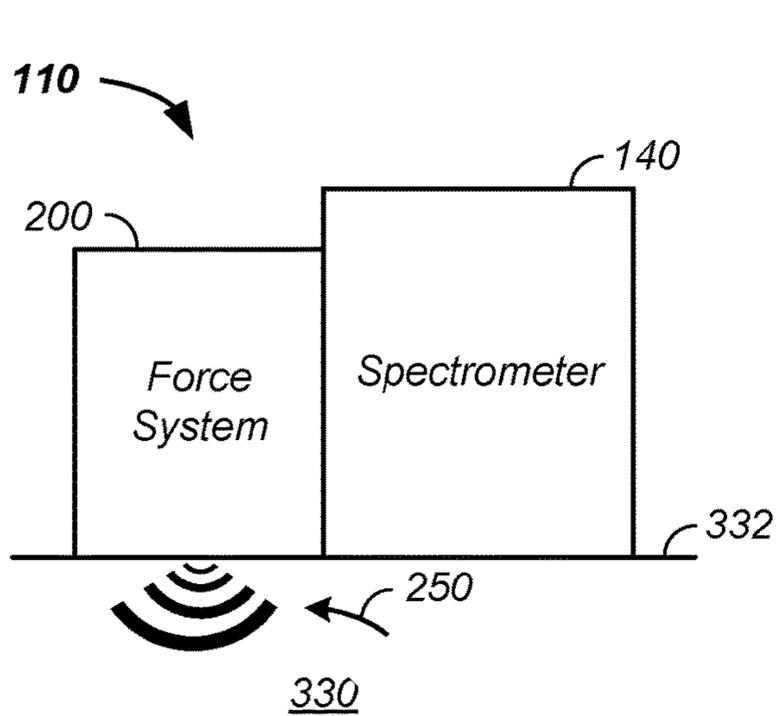


FIG. 5A

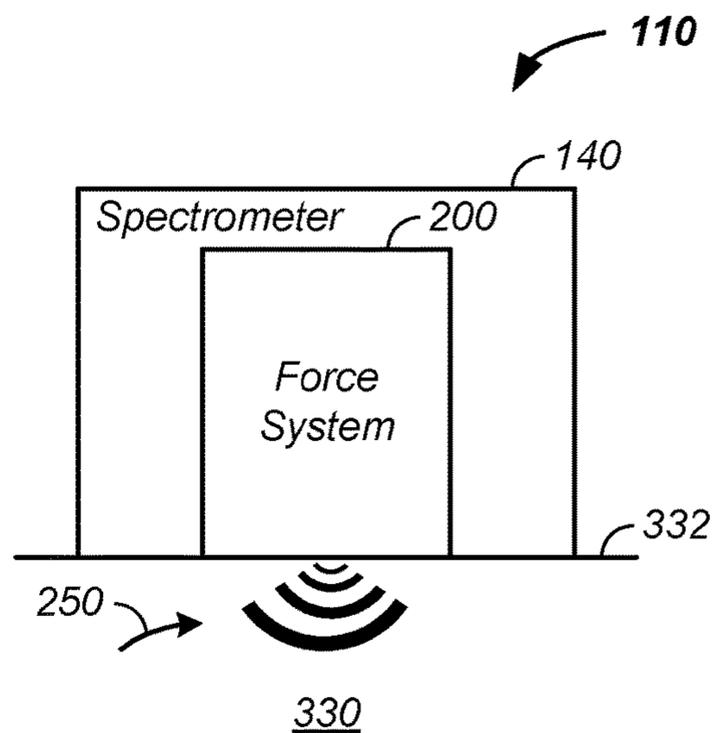


FIG. 5B

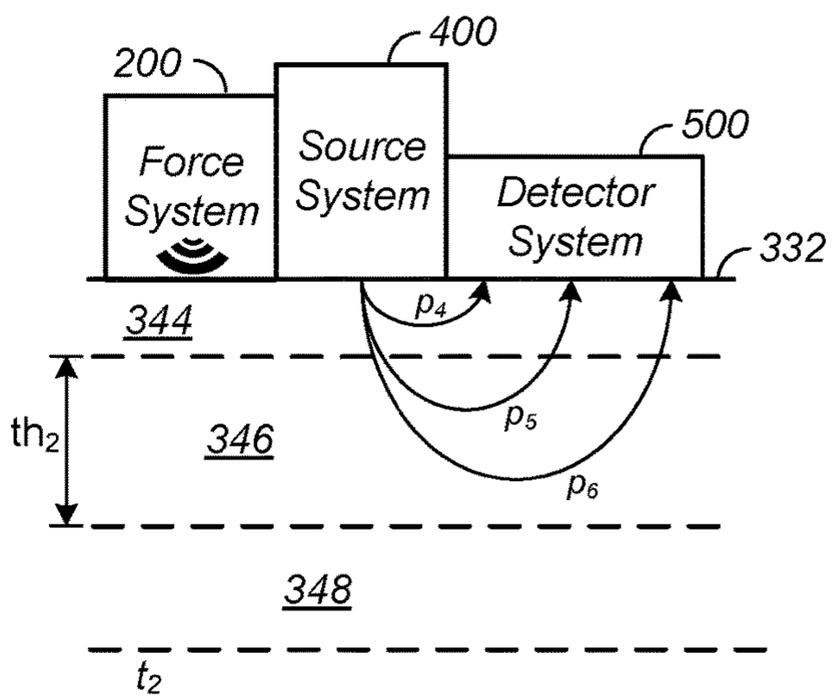
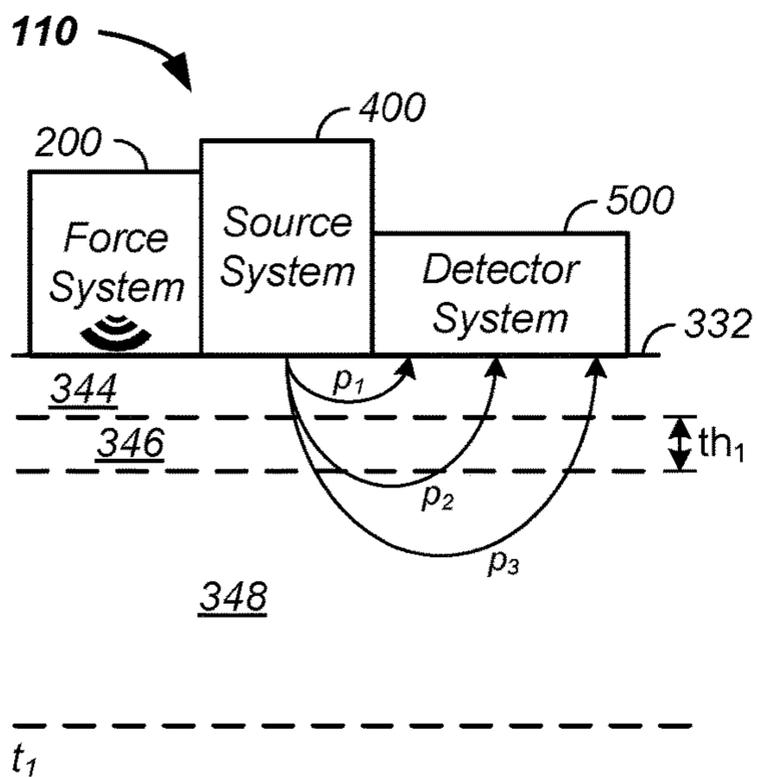


FIG. 6

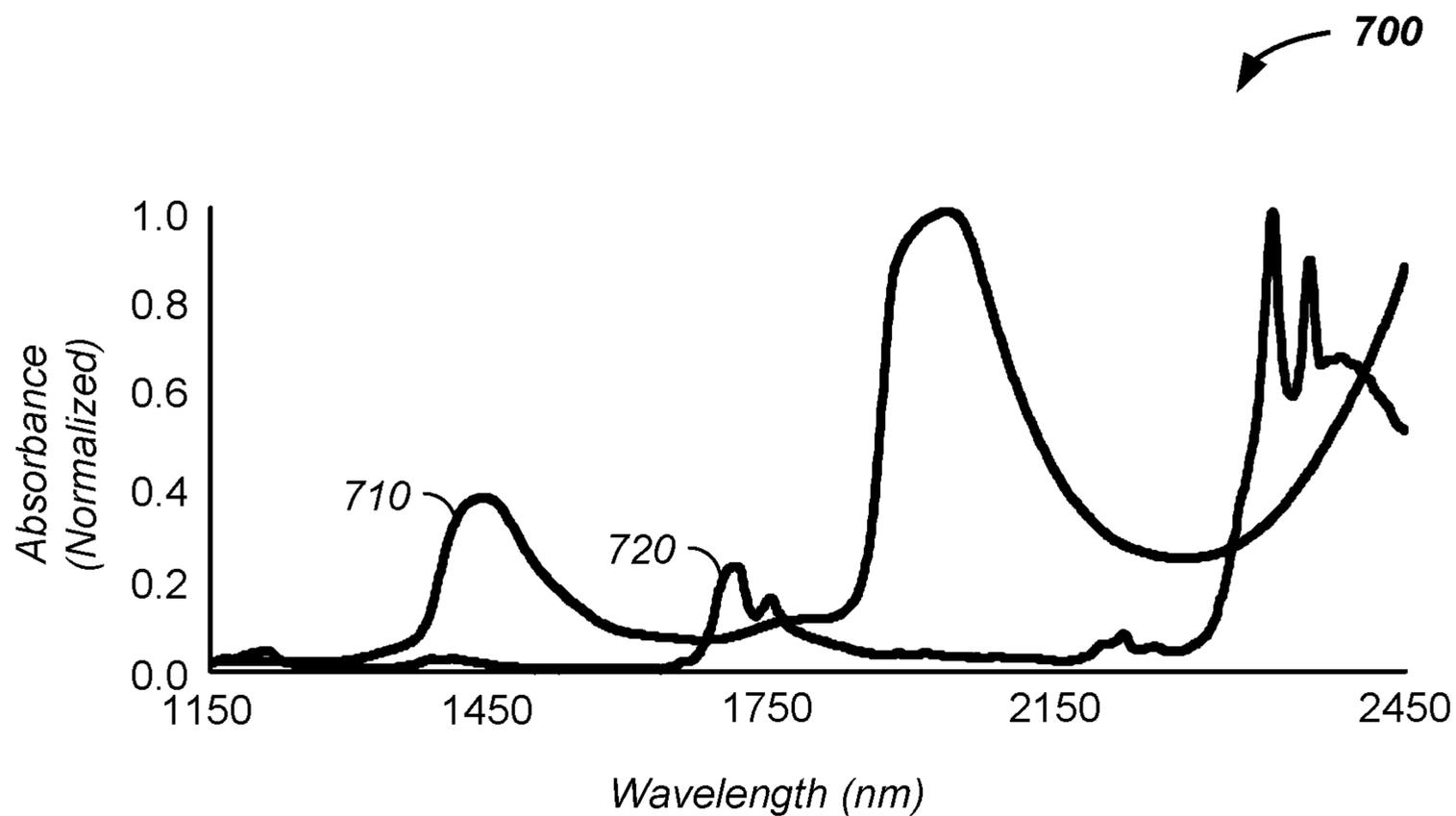


FIG. 7A

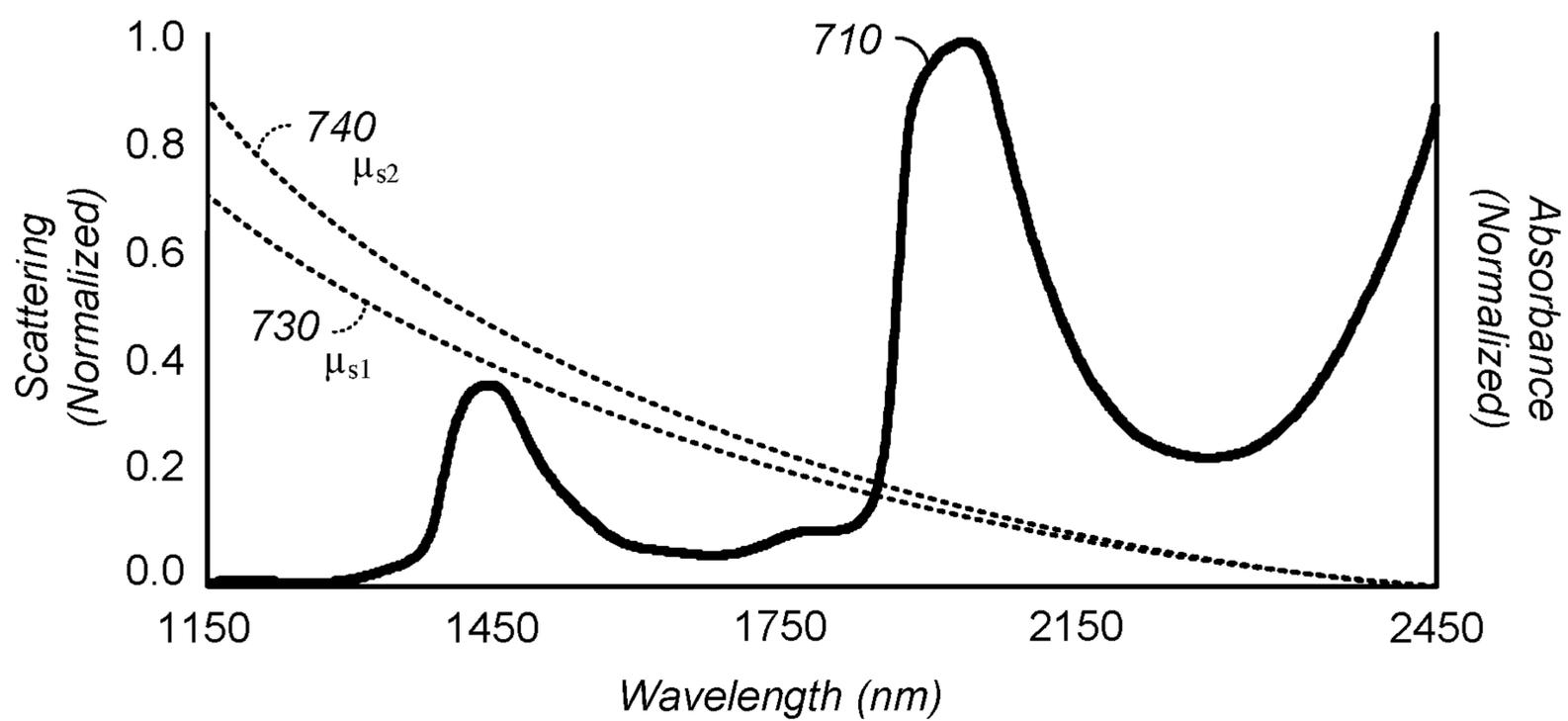


FIG. 7B

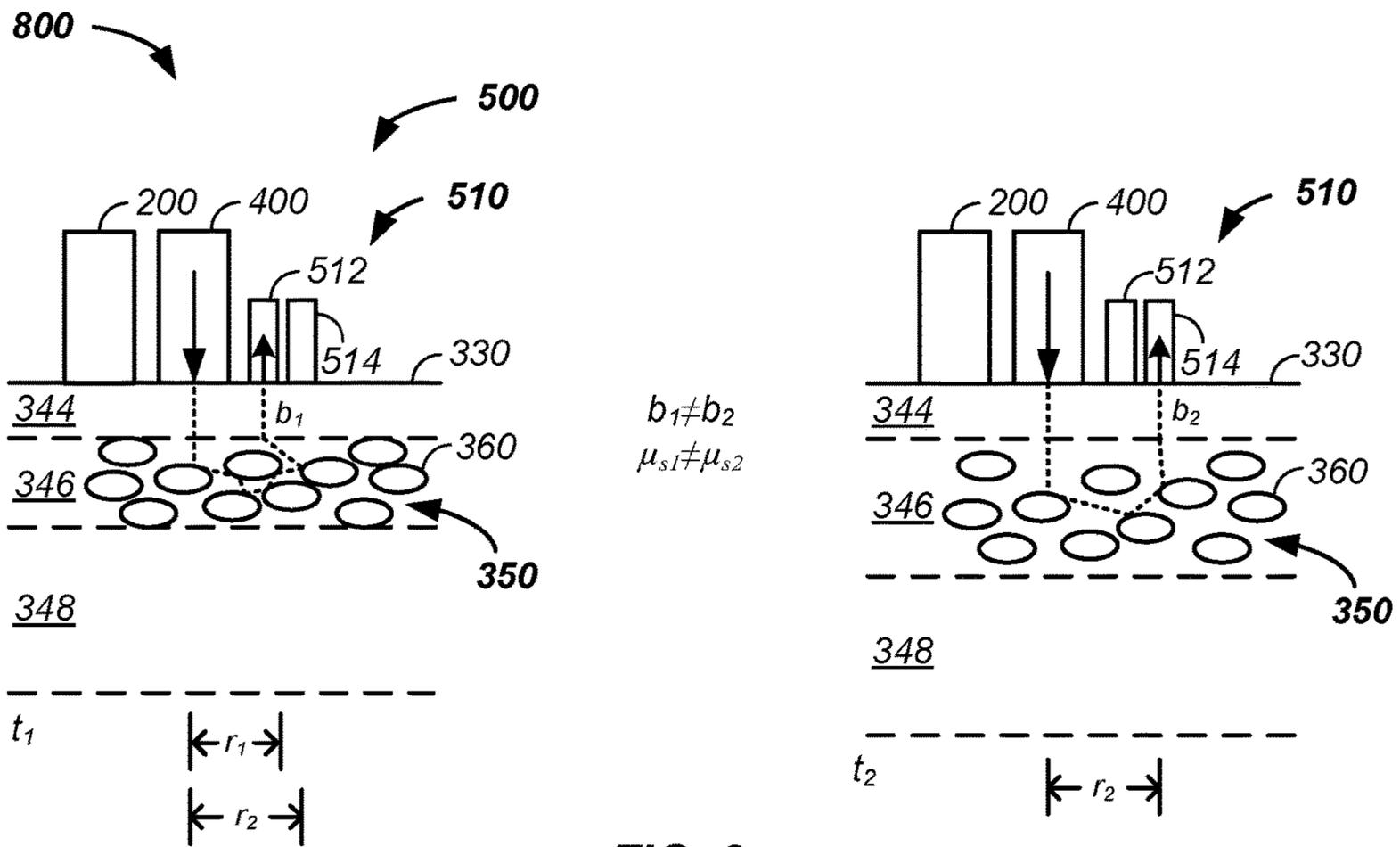


FIG. 8

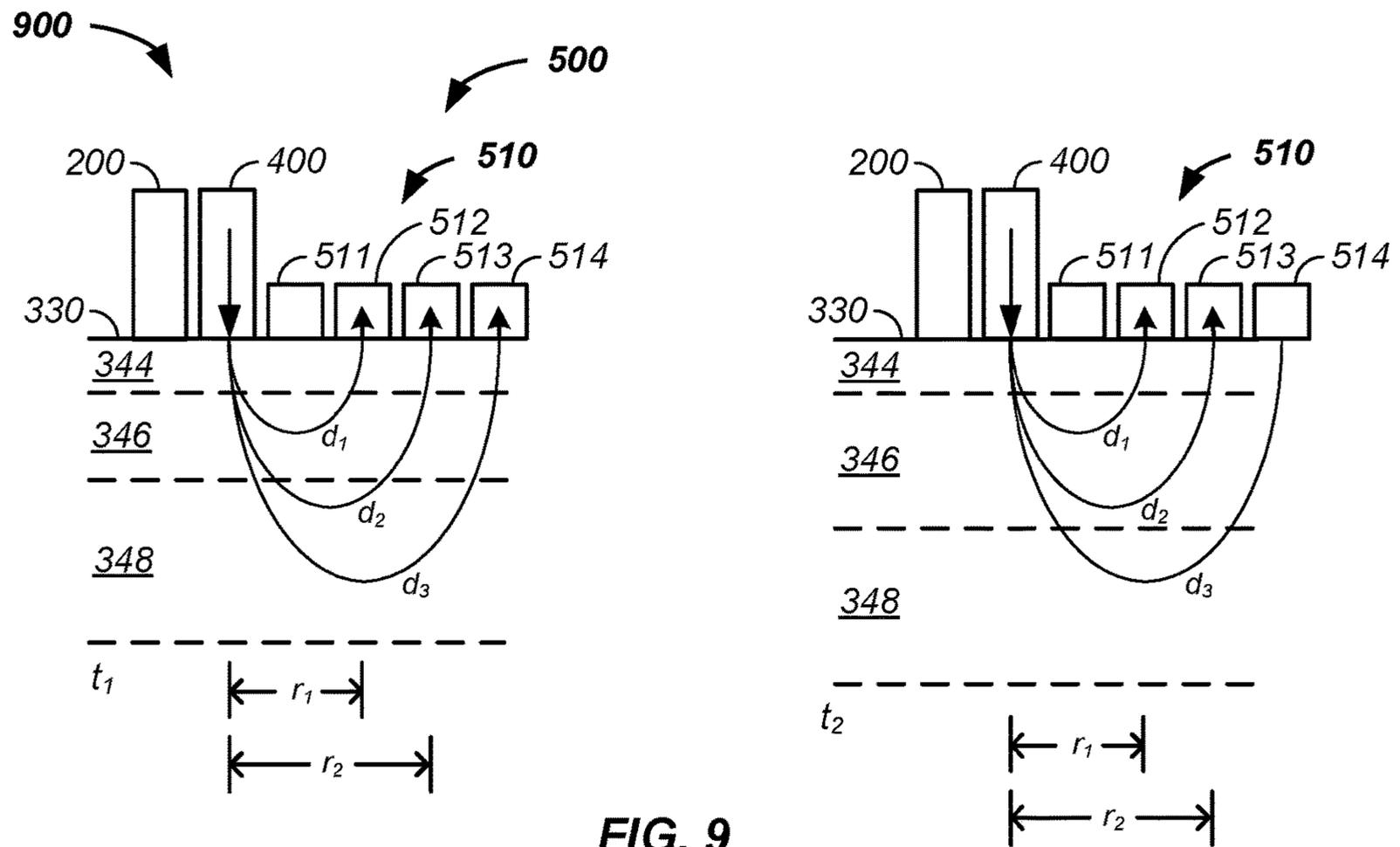


FIG. 9

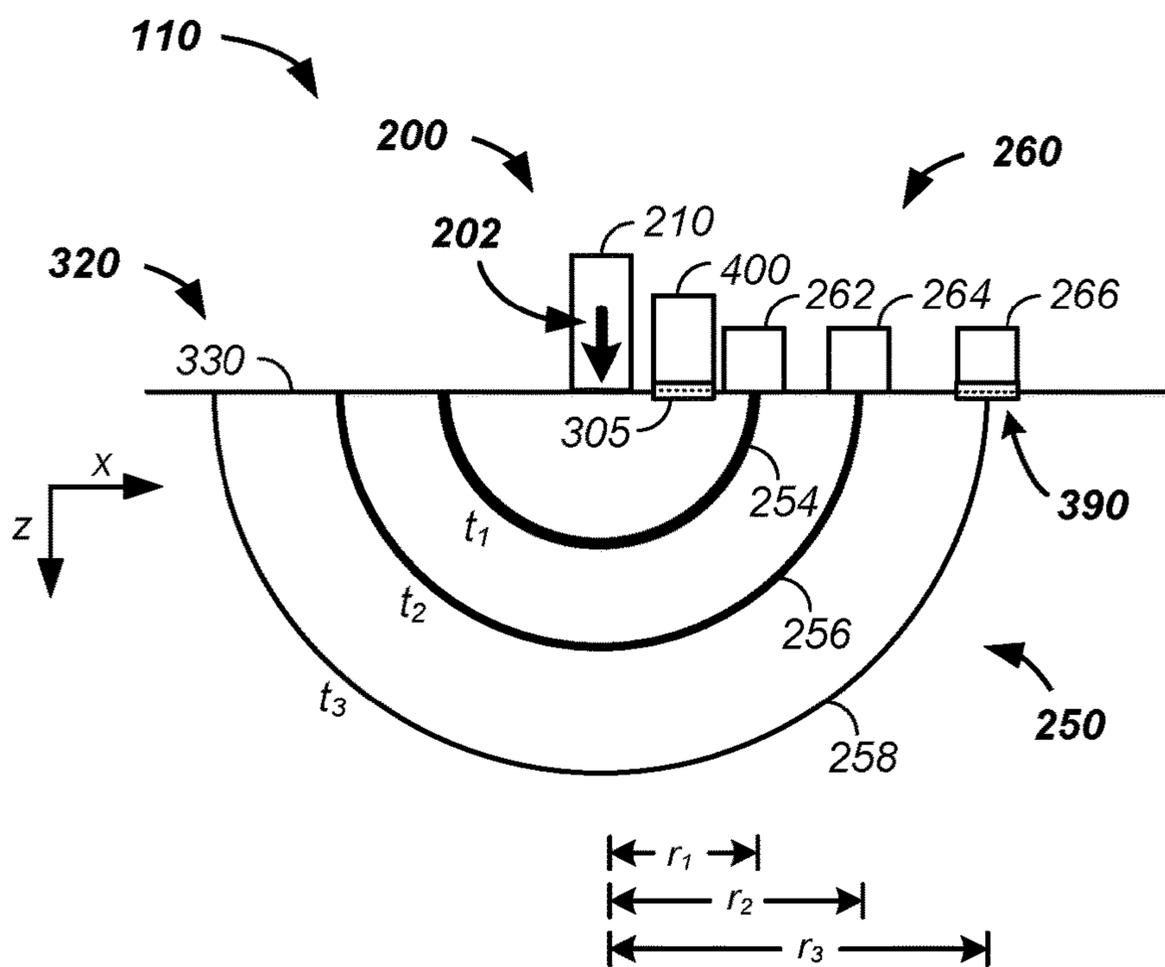


FIG. 10A

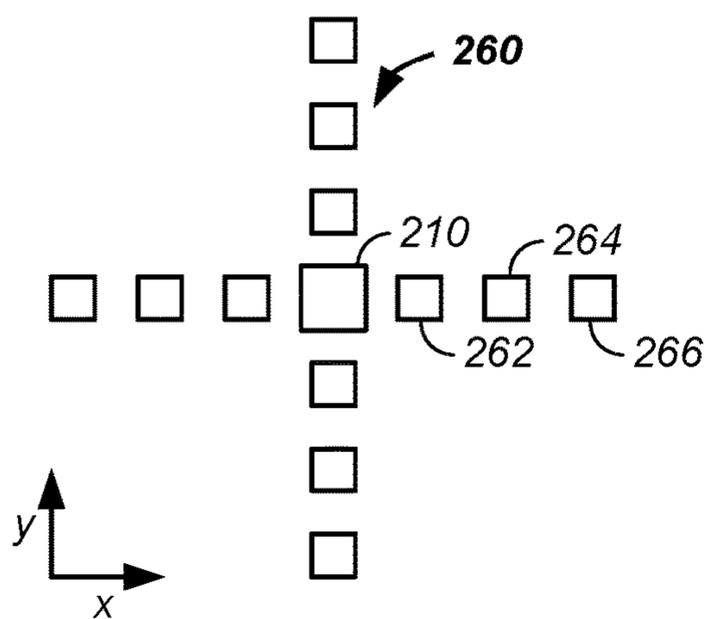


FIG. 10B

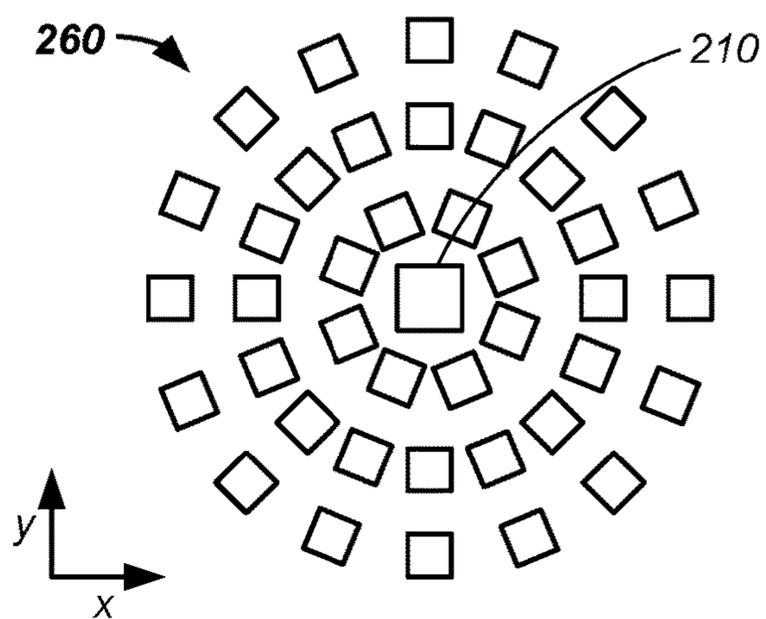


FIG. 10C

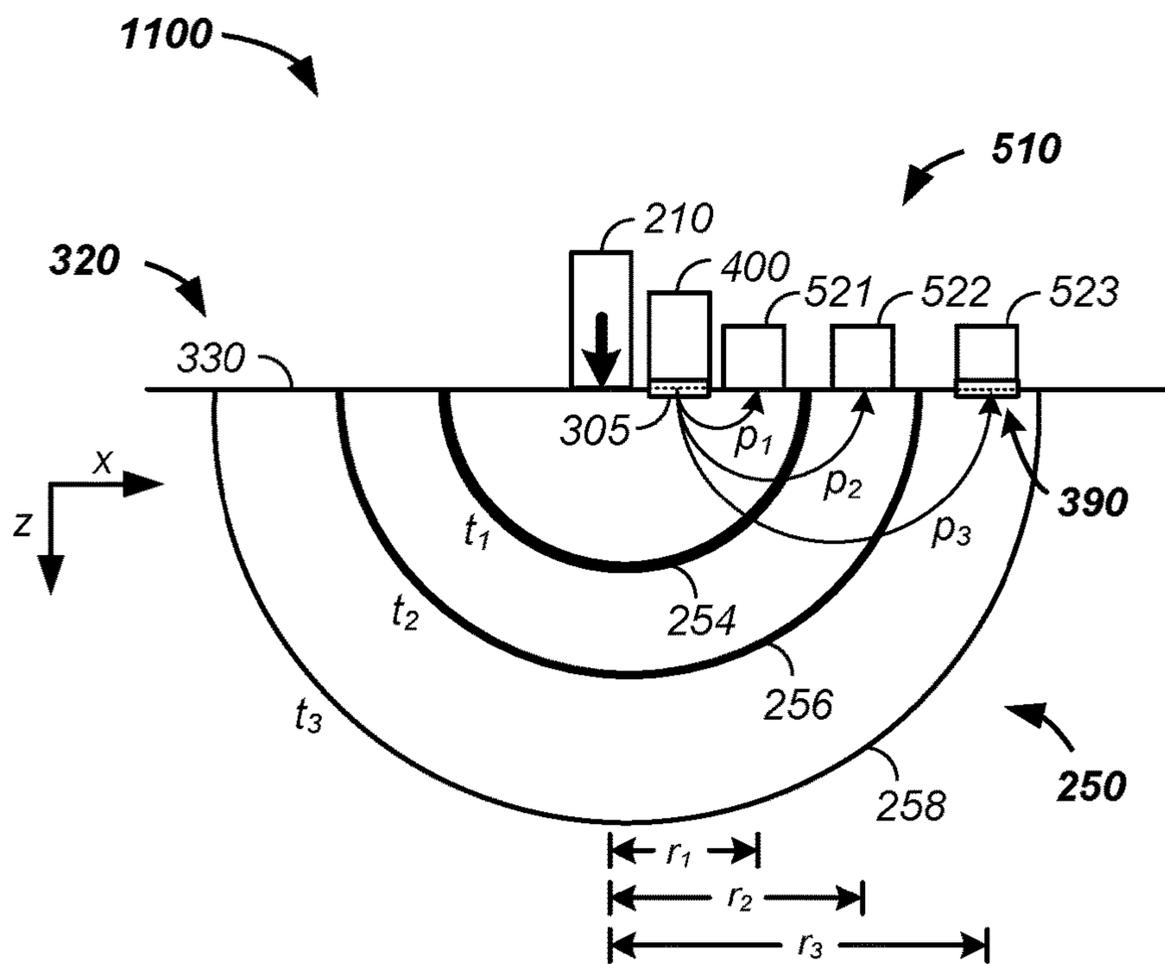


FIG. 11A

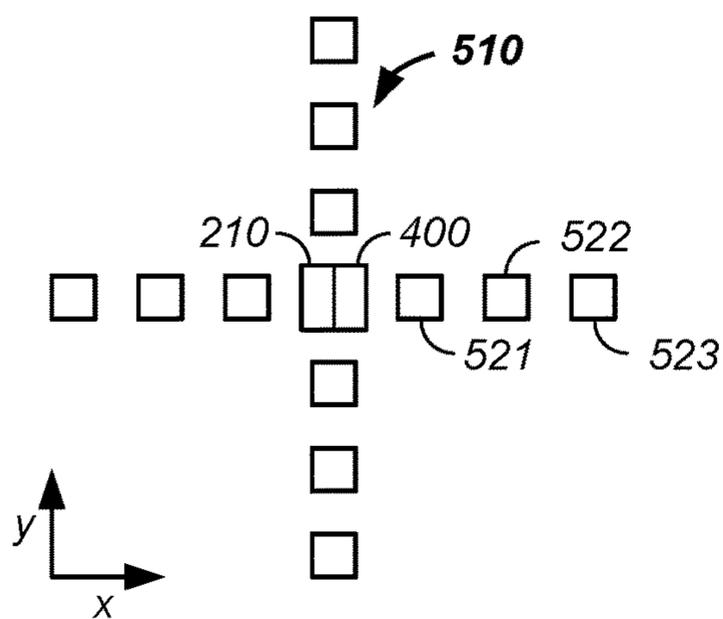


FIG. 11B

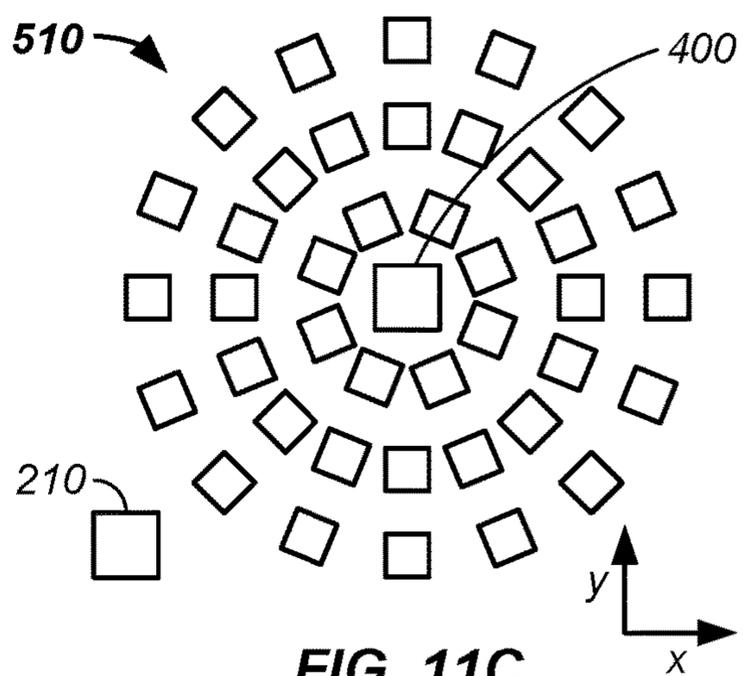


FIG. 11C

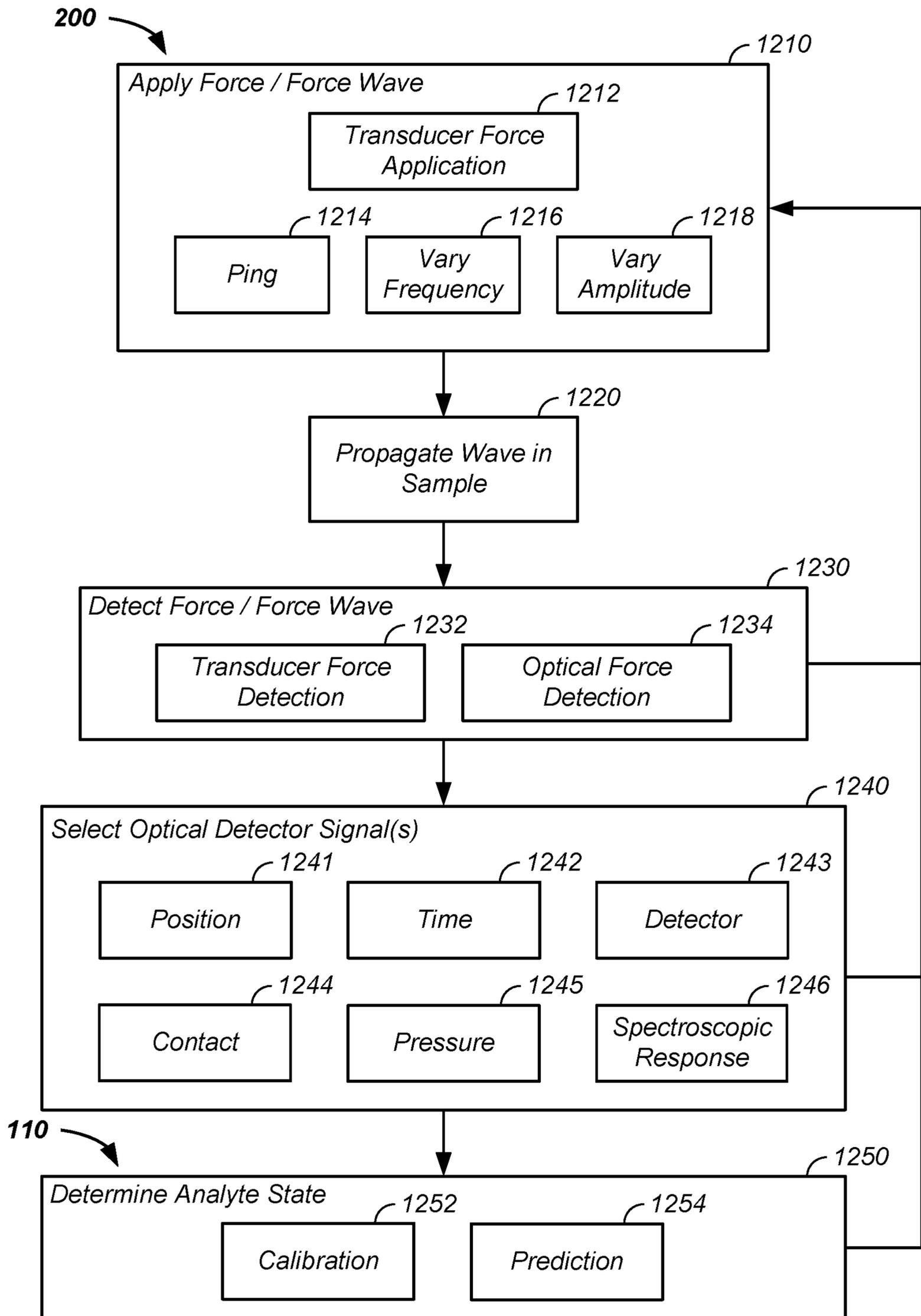


FIG. 12

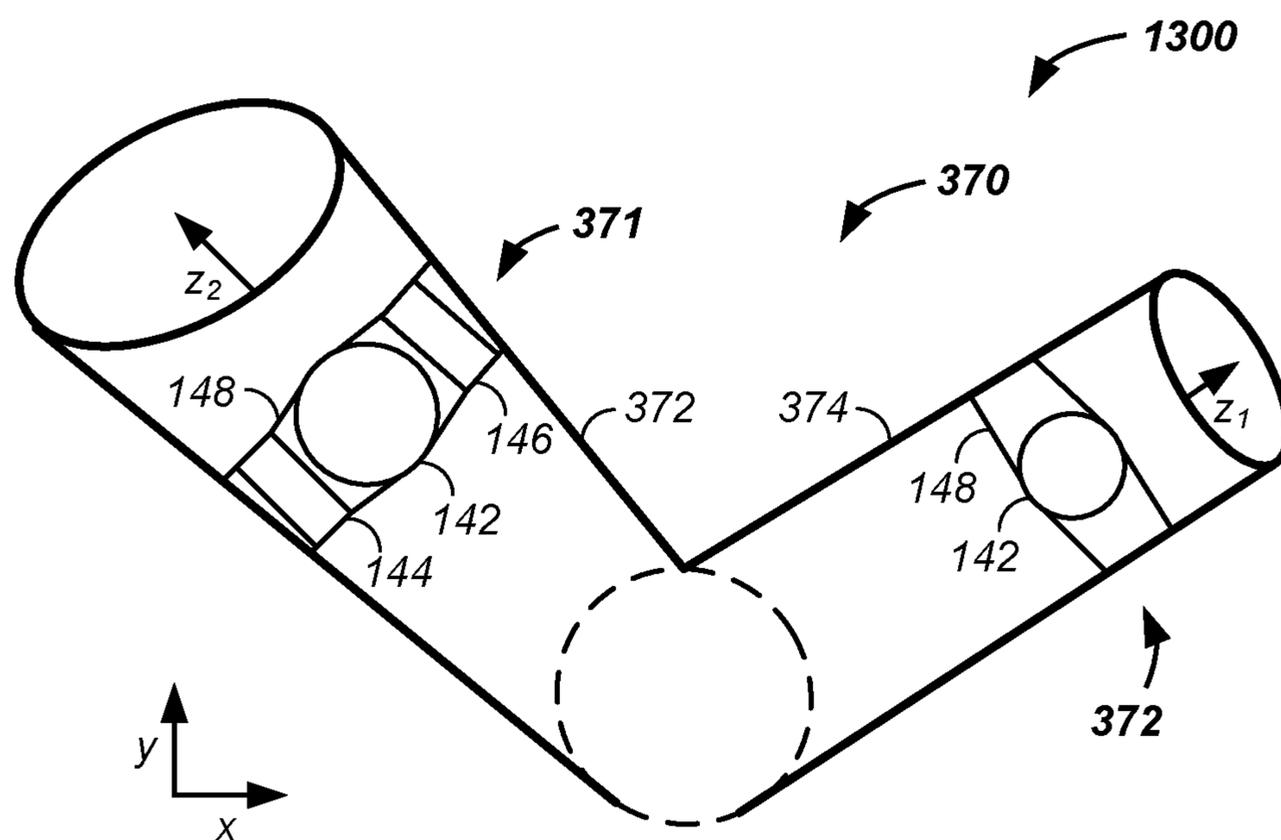


FIG. 13

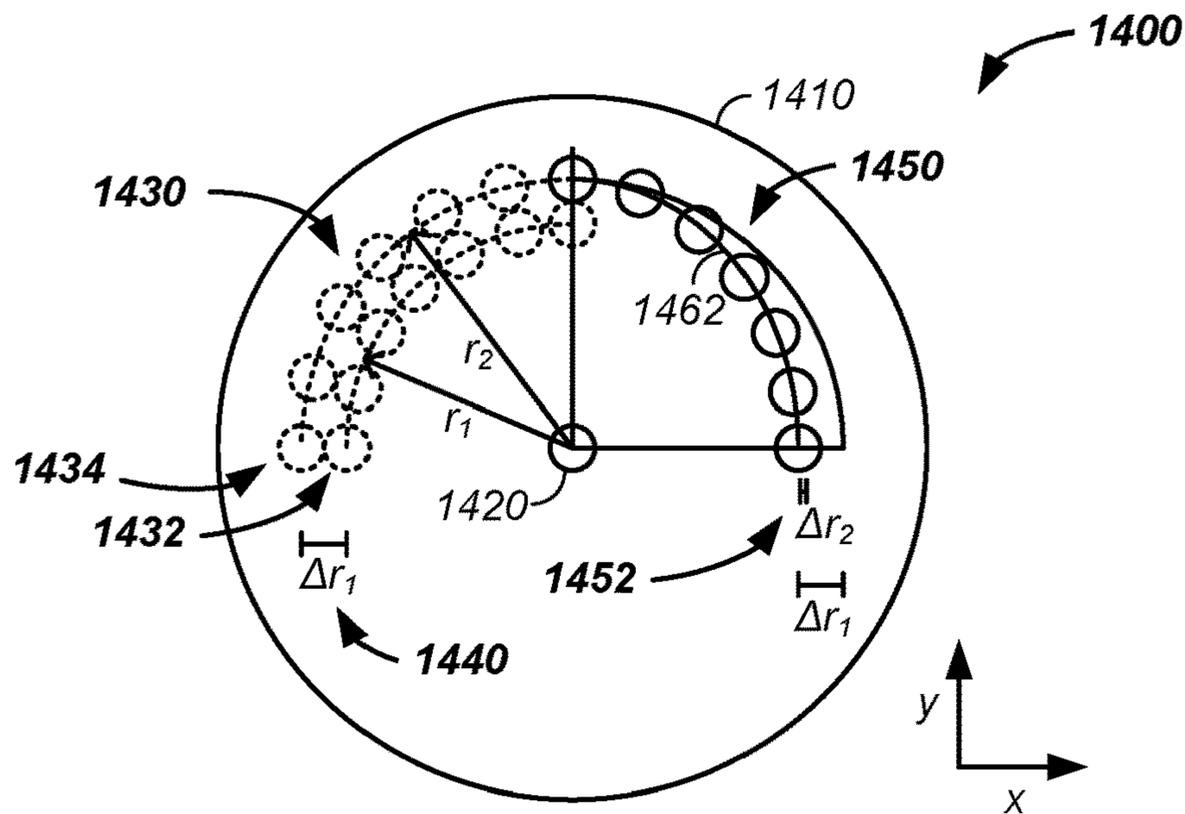


FIG. 14A

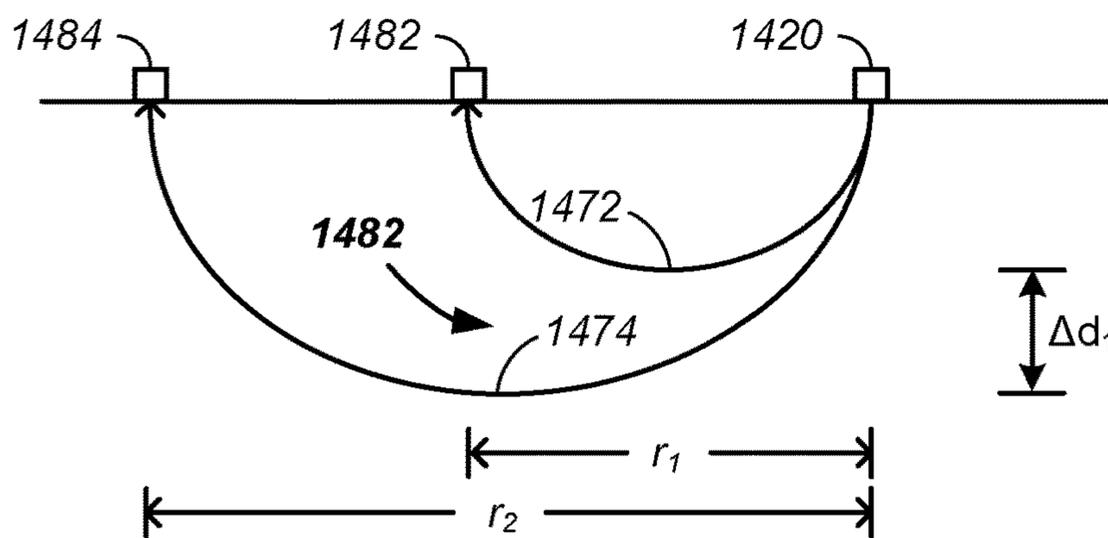


FIG. 14B

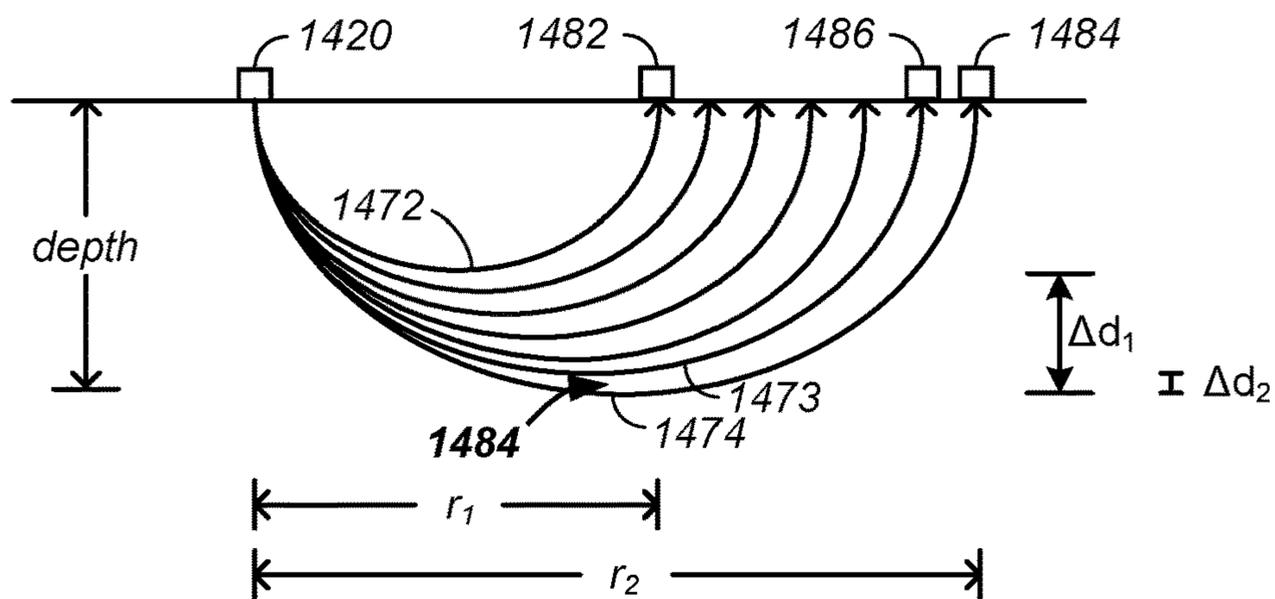


FIG. 14C

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**DEPTH RESOLVED NONINVASIVE
GLUCOSE CONCENTRATION
DETERMINATION ANALYZER APPARATUS
AND METHOD OF USE THEREOF**

CROSS-REFERENCES TO RELATED
APPLICATIONS

This application is a continuation-in-part of U.S. patent application Ser. No. 15/829,877 filed Dec. 2, 2017, which is a continuation-in-part of U.S. patent application Ser. No. 15/636,073 filed Jun. 28, 2017, which claims benefit of U.S. provisional patent application No. 62/355,507 filed Jun. 28, 2016.

BACKGROUND OF THE INVENTION

Field of the Invention

The invention relates generally to noninvasively determining glucose concentration in a living body using an optical analyzer, such as a visible/near-infrared noninvasive glucose concentration determination analyzer.

Discussion of the Prior Art

There exists in the art a need for noninvasively determining glucose concentration in the human body.

SUMMARY OF THE INVENTION

The invention comprises a noninvasive glucose concentration analyzer apparatus and method of use thereof.

DESCRIPTION OF THE FIGURES

A more complete understanding of the present invention is derived by referring to the detailed description and claims when considered in connection with the Figures, wherein like reference numbers refer to similar items throughout the Figures.

FIG. 1 illustrates use of an applied force-optic analyzer; FIG. 2 illustrates a noninvasive analyzer;

FIG. 3A illustrates an applied force system, FIG. 3B illustrates a transducer, FIG. 3C illustrates transducer movement normal to an optical axis, FIG. 3D illustrates a z-axis transducer, and FIG. 3E illustrates a multi-axes off-center spinning mass transducer;

FIG. 4A illustrates spectrometer components, FIG. 4B illustrates an affixing layer, and FIG. 4C illustrates a coupling fluid enhanced affixer;

FIG. 5A illustrates a force system coupled to a spectrometer and FIG. 5B illustrates a force system embedded in a spectrometer;

FIG. 6 illustrates photons interacting with applied force wave(s) in tissue;

FIG. 7A illustrates absorbance of skin constituents and FIG. 7B illustrates scattering;

FIG. 8 illustrates detector selection;

FIG. 9 illustrates changing detector selection with tissue change;

FIG. 10A illustrates a transducer force applicator and FIG. 10B and FIG. 10C illustrate transducer force detectors in lines and arcs respectively;

FIG. 11A illustrates radial optical detection of force waves, FIG. 11B illustrates an array of optical detectors, and FIG. 11C illustrates arcs of optical detectors;

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FIG. 12 illustrates optical probes observing tissue modified by force waves in a noninvasive glucose concentration determination system/analyzer;

FIG. 13 illustrates a multi-sensor analyzer system; and

FIG. 14A illustrates spirally distributed detectors, FIG. 14B illustrates a first depth resolved system, and FIG. 14C illustrates an enhanced depth resolution system.

Elements and steps in the figures are illustrated for simplicity and clarity and have not necessarily been rendered according to any particular sequence. For example, steps that are performed concurrently or in different order are illustrated in the figures to help improve understanding of embodiments of the present invention.

Problem

There remains in the art a need for a noninvasive glucose concentration analyzer.

DETAILED DESCRIPTION OF THE
INVENTION

The invention comprises a method and apparatus for noninvasively determining a sample property, comprising the steps of: a main controller of an analyzer controlling photon generation from a source and analyzing signal from a set of detectors; irradiating an illumination zone of skin with the photons; and detecting a portion of the current set of photons, after passage through the skin, the set of detectors respectively optically coupled to a set of detection zones of the skin positioned along a spiral path from a first radial distance from the illumination zone to a second radial distance from the illumination zone, where a first detection zone of a first detector of the set of detectors extends radially outward from the illumination zone to at least an inward radial distance, from the illumination zone, of a second detection zone of a second detector of the set of detectors, where at least one detection zone of the set of detection zones has a central radial distance from the illumination zone between the first and second radial distances, the main controller selecting current signals from a first subset of the set of detectors for determination of the sample constituent property.

Herein, generally, when describing an optical portion of the applied force-optic analyzer, a z-axis is aligned with a mean direction of the photons in a given sub-portion of the analyzer, such as along a longitudinal path of the photons into skin of a subject, and x- and y-axes form a plane perpendicular to the z-axis, such as at an interface point of incident photons into the skin of the subject. At the point of contact of the applied force-optic analyzer with the biological sample, the z-axis is normal/perpendicular to the sample and the x/y-plane tangentially contacts the sample. For instance, the light moves dominantly along the z-axis along vectors approaching perpendicular to an upper arm of a subject or a patient and the x/y-plane tangentially touches the upper arm along the z-axis. In particular cases, a second x, y, z-axis system is used to describe the sample itself, such as a z-axis being along the longitudinal length of a body part, such as along a digit or a finger or along the length of an arm section and the x/y-plane in this case is a cross-section plane of the body part.

A sample is optionally any material responding to an applied physical force in a manner observed by a probing optical system. However, for clarity of presentation and without loss of generality, the sample is described as a person, subject, patient, and/or a living tissue, such as skin

and/or a portion of a human or animal. While the analyzer is described as a noninvasive analyzer probing into and optionally through the outer layers of skin, the noninvasive analyzer is optionally used as and or in conjunction with a minimally invasive glucose concentration analyzer and/or in conjunction with an invasive glucose concentration analyzer.

Herein, an illumination zone and/or an imaging zone is a point, region, or area of intersection of the illumination/imaging beam and/or pulse with an incident surface of the sample to yield a spectrum and/or an image of a desired volume of the sample. Herein, a detection zone is a point, region, or area of the sample sampled and/or visualized by one or more detectors. Similarly, herein an applied force zone is an incident point, region, or area of intersection at which an applied force is applied to the sample and a detected force zone is a point, region, or area of the sample interfacing with a force detector.

Applied Force-Optic Analyzer

Referring now to FIG. 1, a noninvasive analysis system **100** using an analyzer **110**, such as an applied force-optic analyzer system is illustrated. Generally, an optional force system **200** is used to apply one or more applied forces, physical distortions, and/or force waves to a sample **300**. The applied force travels with a wave front, as a wave, in a pattern of compression and rarefaction, and/or as a traveling displacement through the sample **300** or portions thereof. With or without application of the force waves, a spectrometer **140** is used to noninvasively collect spectra of the sample **300** and photometrically determine one or more properties of the sample, such as a glucose concentration. As described infra, the applied force is optionally in the form of an acoustic wave. However, the applied force is optionally and preferably a physical displacement of a portion of skin of a person, where the physical displacement is caused by movement of a mechanical object relative to the body to yield a time varying displacement of skin and/or constituents of the skin by the mechanical object. As described, infra, a variety of force provider technologies are available to variably displace the skin in a controlled manner. For clarity of presentation and without loss of generality, a transducer is used as an example to represent an applied force section of the force system **200**, where a transducer comprises a device that receives a signal/force in the form of one type of energy and converts it to a signal/force in another form. Again for clarity of presentation and without loss of generality, a piezoelectric actuator is used to represent a transducer and an off-center spinning mass is used to represent a transducer. Hence, again for clarity of presentation and without loss of generality, a piezoelectric-optical analyzer or simply a piezo-optic analyzer, a transducer, and/or a transducer force applicator is used to describe any and all applied force electromechanical sources in the force system **200**.

Referring now to FIG. 2, use of the analyzer **110** is described. Generally, the analyzer **110** is optionally calibrated using a reference **310** and is used to measure a subject **320**, where the subject **320** is an example of the sample **300**. Optionally and preferably, the analyzer **110** and/or a constituent thereof communicates with a remote system **130** using a wireless communication protocol **112** and/or a wired communication protocol.

Force System

Referring now to FIGS. 3(A-E), the force system **200** is further described. Generally, the force system **200** comprises a force delivery transducer that directly and/or indirectly contacts the sample **300**, such as an outer skin surface **330** of the subject **320** and/or a patient. The subject **320** has many

skin layers **340**, which are also referred to herein as tissue layers. For clarity of presentation, the skin layers **320** are represented as having a first skin layer, such as a stratum corneum **342**; a second skin layer, such as an epidermis **344** or epidermal layer; a third skin layer, such as a dermis **346** or dermis layer; and a fourth layer, such as subcutaneous fat **348** or a subcutaneous fat layer. It is recognized that skin is a complex organ with many additional layers and many sub-layers of the named layers that vary in thickness and shape with time. However, for clarity of presentation and without loss of generality, the stratum corneum, epidermis, dermis, and subcutaneous fat layers are used to illustrate impact of the force delivery transducer on the skin layers **340** of the subject **320** and how the applied force waves alter optical paths of probing photons in the spectrometer **140** of the analyzer **110** in the noninvasive analysis system **100**.

Still referring to FIG. 3A, at a first time, t_1 , the tissue layers **340** are in a first state. As illustrated, the tissue layers **340** are in a compressed state **340**, such as a result of mass of the force system **200** sitting on the skin surface **330**, as a result of dehydration of the subject **320**, and/or as a result of a physiological and/or environmental force on the tissue layers **340** of the subject. At a second time, t_2 , the force system **200** applies a force wave **250** to the skin surface **330** of the patient **320**, which sequentially propagates into the stratum corneum **342**, epidermis **344**, dermis **346**, and given enough force into the subcutaneous fat **348**. In addition to the force wave propagating into the skin layers **340** along the z-axis, the force wave propagates radially through the skin layers, such as along the x/y-plane of the skin layers. As illustrated at the second time, t_2 , as the force wave **250** propagates into the tissue layers **340**, the tissue layers expand and/or rarefy, such that the thickness of the epidermis **344** and/or the dermis **346** layers expands. The rarefaction of the epidermis **344** and particularly the dermis **346** allows an increased and/or enhanced perfusion of blood **350** into the rarefied layers. The increased perfusion increases water concentration in the perfused layers, increase and/or changes distance between cells in the perfused layers, and/or changes shapes of cells in the perfused layers, such as through osmolarity induced changes in concentration in and/or around blood cells, such as red blood cells. Generally, scattering coefficients of the epidermis layer and/or especially the dermis layer changes, which is observed by the spectrometer **140** in the range of 400 to 2500 nm with larger changes at smaller wavelengths in the visible, 400 to 700 nm, and/or near-infrared, 700 to 2500 nm, regions. As illustrated at the third time, t_3 , as the force wave **250** continues propagation in the tissue layers **340**, the perfusion **350** continues to increase, such as to a maximum perfusion. As illustrated at the fourth time, t_4 , after discontinuation of the force wave **250**, the skin layers **340** revert toward the initial state of the non-force wave induced perfusion to a local minimum perfusion, which may match the initial perfusion, is likely higher than the initial perfusion, and is at times less than the initial perfusion due to changes in state of the environment, such as temperature, and/or generalized state of the subject **320**, such as hydration, localized hydration of skin, such as due to food intake, insulin response to food intake, exercise level, blood pressure, and/or the like. Generally, the tissue layers **340** of the subject increase in thickness and/or rarefy during application of the transducer applied force wave **250** and decrease and/or compress after termination of the transducer applied force wave **250** to the skin surface **330** of the subject **320**. The process of applying the force wave **250** is optionally and preferably repeated n times, where n is a positive integer of greater than 1, 2, 5, 10,

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100, 1000, or 5000 times in a measurement period of an analyte of the subject 320, such as a glucose concentration. Generally, the cycle of applying the force wave 250 results in a compression-rarefaction cycle of the tissue that alters an observed scattering and/or absorbance of probing photons in the visible and near-infrared regions. The force wave 250 is optionally and preferably applied as a single ping force in a tissue state classification step, as multiple pings in a tissue classification step, and/or as a series of waves during a tissue measurement step. Individual waves of a set of force waves are optionally controlled and varied in terms of one or more of: time of application, amplitude, period, frequency, and/or duty cycle.

Still referring to FIG. 3A and referring now to FIGS. 3(B-D), a force wave input element 210 of the force system 200 is illustrated. As illustrated, the force wave input element 210 is equipped with one or more transducers: a left transducer 221, a right transducer 222, a front transducer 223, a back transducer 224, a top transducer 225, and/or a bottom transducer 226. For instance, the left and/or right transducers 221, 222 move the force wave input element 210 left and/or right along the x-axis; the front and/or back transducers 223, 224 move the force wave input element 210 forward and/or back along the y-axis; and/or the top and bottom transducers 225, 226 move the force wave input element 210 up and/or down along the z-axis along and/or into the skin surface 330 of the subject 320, which moves the skin, skin layers 340, and/or skin surface 330 of the subject relative the spectrometer 140 and/or is a source of the force wave 250 moving, in the skin layers 340, along the z-axis into the skin, and/or radially outward from an interface zone of the force wave input element 210 of the force system 200. A transducer itself is optionally used as the force wave impulse element 210. Referring now to FIG. 3E, one or more off-center mass elements 230 is optionally spun or rotated, such as with an electric motor, along one or more of the x, y, z-axes to move the force wave input element 210 relative to the skin surface 330 of the subject 320 resulting movement of the skin of the subject 320 relative to the spectrometer 140 and/or cycling and/or periodic displacement of the tissue layers 340 of the subject 320 due to movement of the force wave input element 210 resulting in the force wave(s) 250. Generally, the force system 200 induces a movement of a sampled zone of skin of the subject 320, applies a displacement of a sampled zone of the skin of the subject 320, and/or applies a propagating force wave into and/or through a sample zone of tissue layers 340 of the subject, where the sampled zone is probed using photons from the spectrometer 140 and/or is measured using a set of detection zone transducers, described infra. The force wave(s) are optionally and preferably applied as a single input ping wave, a set of input ping waves, and/or are applied with a frequency of 0.01 Hz to 60 Hz. Optionally and preferably, the force waves 250 are applied with a frequency greater than 0.01, 0.02, 0.05, 0.1, or 1 Hz. Optionally and preferably, the force waves 250 are applied with a frequency of less than 200, 100, 50, 40, 30, or 20 Hz. Optionally and preferably, the force waves 250 are applied with a frequency within 5, 10, 25, 50, or 100 percent of 2, 4, 6, 8, 10, 12, 15, and 20 Hz.

Optical System

Referring now to FIG. 4A, the spectrometer 140 of the analyzer 110 is further described. The spectrometer 140 comprises a source system 400, which provides photons 452 in the visible and/or infrared regions to the subject 320, such as via a photon transport system 450, at an illumination zone. After scattering and/or absorbance by the tissue layers 340 of the subject 320, a portion of the photons are detected

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at a detection zone by a detector system 500. The source system 400 includes one or more light sources, such as any of one or more of a light emitting diode, a laser diode, a black body emitter, and/or a white light source, that emits at any wavelength, range of wavelengths, and/or sets of wavelengths from 400 to 2500 nm. Each source system photon source is optionally controlled in terms of time of illumination, intensity, amplitude, wavelength range, and/or bandwidth. The photon transport system 450 comprises any fiber optic, light pipe, air interface, air transport path, optic, and/or mirror to guide the photons from the light source to one or more illumination zones of the skin surface 330 of the subject 320 and/or to guide the photons from one or more detection zones of the skin surface 330 of the subject 320 to one or more detectors of the detector system 500. Optionally and preferably, the photon transport system 450 includes one or more optical filters and/or substrates to selectively pass one or more wavelength regions for each source element of the source system 400 and/or to selectively pass one or more wavelength ranges to each detector element of the detector system 500. Herein, the reference 310 is optionally an intensity and/or wavelength reference material used in place of the sample and/or is used in a optical path simultaneously measured by the analyzer 110.

Still referring to FIG. 4A and referring now to FIG. 4B and FIG. 4C, the subject 320 optionally and preferably wears the analyzer 110 in the physical form of a watch head, band, and/or physical element attached to the body with a band and/or an adhesive. For example, the analyzer 110, the spectrometer 140, the source system 400, and/or the photon transport system 450 is optionally attached to the subject 320, such as at the wrist or upper arm, using thin affixing layer 460, such as a double sided adhesive 462. Referring now to FIG. 4B, the double sided adhesive 462 optionally contains an aperture 464 therethrough. The photons 452 optionally and preferably pass through the aperture 452 to the skin surface 330 of the subject. The force wave 250 optionally moves the skin surface 330 through the aperture into intermittent contact with the analyzer 110. Optionally, referring now to FIG. 4C, a thin affixing layer 466, such as less than 1, 0.5, or 0.25 mm thick, is continuous in nature in front of the incident surface and/or incident photon coupling zone and/or is continuous in nature in front of the detection zone, where photons exiting the skin surface 330 are detected by the detector system 500. The affixing layer 466 is optionally permeated with a fluid, such as a coupling fluid, an air displacement medium, an optical coupling fluid, a fluorocarbon liquid, a fluorocarbon gel, an index of refraction matching medium, and/or any fluid that increases a percentage of photons from the source system 400 entering the skin surface 330 compared to an absence of the fluid and/or is any fluid that increases a percentage of photons from the tissue layers 340 exiting the detection zone and reaching the detector system 500 as compared to a case where the fluid is not embedded into the affixing layer. Hence, the affixing layer serves several purposes: attaching the analyzer or a portion thereof to the skin surface 330 of the subject 320, coupling forces from the force system 200 to the skin surface 330 of the subject 320, forming a constant sampling interface location on the skin surface 330 of the subject, and/or altering a coupling efficiency, angular direction, and/or reproducibility of coupling of photons enter the skin of the subject 320 and/or exiting the skin surface 330.

Coupled Force System/Spectrometer

Referring now to FIG. 5A and FIG. 5B, the force system 200 is illustrated working in conjunction with the spectrometer 140. Referring now to FIG. 5A, the analyzer 110 is

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illustrated with the force system **200** being attached to and/or within 1, 2, 3, 5, 10, 20, or 50 mm of the spectrometer **140**. Referring now to FIG. **5B**, the analyzer **110** is illustrated with the force system **200** being integrated into the spectrometer **140**, such as within 20, 10, 5, 2, or 1 mm of the source system **400** of the analyzer **110** and/or in a single housing unit of the analyzer **110**.

Several examples are provided that illustrate how the force system **200** alters the tissue layers **340** of the subject **320** and how a selection of detected signals from the spectrometer **140** is performed as a function of time and respective radial separation between the one or more illumination zones and the one or more detection zones, such as using water signal, fat signal, and/or protein signal to determine the correct detection signals to use for noninvasive glucose concentration determination.

Example I

Referring now to FIG. **6**, a first example of the analyzer **110** using the force system **200** and the source system **400** at the same time and/or within less than 60, 30, 15, 10, 5, or 1 second of each other is provided. In this example, the force system **200** applies a force to the tissue layers **340** at a first time, t_1 , when the dermis has a first mean z-axis thickness, th_1 . Optionally and preferably, the analyzer **110** acquires signals representative of the tissue layers **340** of the subject **320** using the source system **400** and the detector system **500**. Illustrated are three representative photon pathways, p_{1-3} , reaching the detector system **500**, such as at a first detector element, a second detector element, and a third detector element, respectively, at the first time, t_1 , and/or within less than 60, 30, 15, 10, 5, or 1 second from the first time, t_1 . Notably, at the first time, the first photon pathway, p_1 , has an average path that does not penetrate into the dermis **346**, while the second and third photon pathways, p_{2-3} , have mean pathways that penetrate through the dermis into the subcutaneous fat **348**. In at least one preferred use of the analyzer, noninvasive glucose concentration determination is performed using a mean photon pathway that penetrates into the dermis **346** and not into the subcutaneous fat **348** and/or uses signal from a detector element at a first/minimal radial distance from the illumination zone, where the first/minimal radial distance is the smallest radial distance observing an increase in a fat signal/dominantly fat related signal, such as from the subcutaneous fat **348**, compared to a water signal/dominantly water related signal from skin layers **340** closer to the skin surface **332** than that subcutaneous fat **348**. Examples of wavelengths containing dominantly water absorbing signals are wavelengths correlating with the peaks of the water absorbance bands **710**, FIG. **7A**, and examples of wavelengths containing an increased fat absorbance to water absorbance ratio when a mean photon path enters the subcutaneous fat **348** are at the fat absorbance bands **720**. Still referring to FIG. **6**, at a second time, t_2 , the force wave **250** from the force system **200** has expanded the dermis layer to a second thickness, th_2 , which is at least 0.1, 0.2, 0.3, 0.5, 1, 2, 5, 10, 20, or 50% thicker than the first thickness, th_1 , and/or has an increased water absorbance, as measure by the first, second, and/or third detector element of the detector system **500**, representative of the first through third photon pathway, p_{1-3} , in the condition of the larger dermis thickness at the second time, t_2 , as represented by a fourth, fifth, and sixth photon pathway, p_{4-6} . Notably, the fifth and sixth photon pathways, $p_{5,6}$, with the same illumination zone to detection zone radial distance as the first and second photon pathways, p_{1-2} , have

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mean photon pathways that penetrate into the dermis **346** and not into the subcutaneous fat **348**. Thus, the water-to-fat ratio of the observed signal continues to increase with radial distance for the second and third detectors after the force system **200** increased the thickness of the dermis **346** to the second thickness, th_2 . Again, at least one preferred measurement is a measurement with a higher water-to-fat absorbance ratio. In this example, at the second time, the water-to-fat absorbance ratio of the fifth optical path, p_5 , is greater than observed with the second optical path, p_2 , despite have the same source zone-to-detector zone radial distance. Further, in this example a preferred optical signal is from the sixth optical path, th_6 , at the second time, t_2 , with a largest ratio of mean pathlength in the dermis **346** to total mean detected pathlength. FIG. **7B** illustrates increased scattering with decreasing wavelength at a first scattering coefficient, μ_{s1} , **730** and a second scattering coefficient, μ_{s2} , **740**.

Example II

Referring now to FIG. **8**, a second example is provided where the analyzer **110** uses the force system **200** to alter the sample **300** to enhance a noninvasive analyte property determination using the spectrometer **140**. As above, the force system **200** provides one or more force waves **250** into the subject **320**, which alters positions of cells **260** in the dermis **346** relative to the illumination zone of the illumination system **400** and or relative to one or more detection zones associated with a single element detector and/or one or more detectors of an array of detector elements **510**. As illustrated, the cells **360** have a first average intercellular distance at a first time, t_1 , which is altered by application of the force wave **250** to a second average intercellular distance at a second time, t_2 , where the net change in cell position alters detected spectrophotometric absorbance signals at a give detector element of the detector system **500** by greater than 0.01, 0.02, 0.05, 0.1, 0.5, 1, 2, 5, or 10 percent, such as by a change in observed scattering and/or observed absorbance at a fixed radial distance between an illumination zone and a detection zone. Similarly, the average percentage volume of the intercellular fluid **350** in the dermis layer differs by greater than 0.01, 0.02, 0.05, 0.1, 0.5, 1, 2, 5, or 10 percent as a result of the applied force wave(s) **250**. All of a change in thickness, change in observed mean pathlength, change in radial distance of detection, change in mean intercellular spacing, change in scattering, and change in water concentration, related to perfusion, are illustrated between the first time, t_1 , and the second time, t_2 , as a result of the applied force wave **250**. Notably, a selected detector signal from the array of detectors **510** changed from a second detector element **512** at a first radial distance, r_1 , from the illumination zone to a fourth detector element **514** at a second radial distance, r_2 , from the illumination zone based on the above described larger observed water signal-to-observed fat signal ratio and/or as the second pathlength, b_2 , is longer than the first pathlength, b_1 , in the dermis layer. Similarly, absorbances of skin constituents, such as protein, albumin, globulin, keratin, and/or elastin increase relative to fat absorbance for the second pathlength, b_2 , as the mean pathlength spends more time in the dermis layer compared to the subcutaneous fat layer **348**, as described supra.

Example III

Referring now to FIG. **9**, a third example of using the force system **200** to alter properties of the subject **330** to enhance performance of a noninvasive glucose concentra-

tion determination using the spectrometer 140 is provided. In this example, the detector array 510 of the detector system 500 contains n detector elements at differing radial distances from a time correlated illumination zone. For clarity of presentation, the detector array 510 is illustrated with four 5 detector elements: a first detector element 511, a second detector element 512, a third detector element 513, and a fourth detector element 514. At a first time, t_1 , the large water absorbance, protein absorbance, and/or protein and water absorbance-to-fat ratio is observed using the second 10 detector element 512 having a first illumination zone-to-detection zone radial distance, r_1 , and a first mean optical pathway, d_1 , penetrating into the dermis 346 with minimal to no mean penetration into the subcutaneous fat 348. However, at a second time, t_2 , after the provided force wave 250 15 has altered the skin of the subject 320, the third detector element is observed, at a selected detection point in time, to have the largest metric for detector selection, such as a smoothly falling observed intensity with radial distance at a fat absorbance wavelength, where a sudden decrease in 20 observed intensity at the fat absorbance wavelength indicates mean penetration of the observed optical pathway into the subcutaneous fat 348, such as at the second radial distance, r_2 . Notably, the largest radial distance is selected for a given water, protein, and/or fat based metric as at the 25 larger radial distance a difference between a shortest possible pathlength between the illumination zone and the detection zone, the radial distance, is closest to the largest possible observed pathlength, which is based upon a maximum observable absorbance by a detector type for a fixed 30 number of photons. For example, if the maximum observable absorbance is 3.9 and the absorbance per millimeter is 1.3, then a maximum observable pathlength is 3.0 mm. If the observed radial pathlength is 1.5 mm then a first range of observed pathlengths is 1.5 to 3.0 mm with a difference of 1.5 mm. Hence, a first ratio of observed pathlength difference to radial distance is 1:1 (1.5 mm:1.5 mm), which is a 100% error. However, if the observed radial pathlength is 2.5 mm, then a second range of observed pathlengths is 2.5 to 3.0 mm with a difference of 0.5 mm. Hence, a second ratio of observed pathlength difference-to-radial distance is 1:5 40 (0.5 mm:2.5 mm), which is a second pathlength error of 20% or one-fifth of the pathlength error of the first case. In general, the largest radial distance yielding and intensity-to-noise ratio beyond a threshold, such as 0.5, 1, 1.5 or 2, is 45 preferred as error in a range of observed pathlengths decreases, which reduces the error in b, in Beer's Law: equation 1,

$$A = \text{molar absorptivity} * b * C \quad (\text{eq. 1})$$

where b is pathlength and C is concentration, which is central to visible and near-infrared absorbance and/or scattering models used to determine an analyte property, such as a noninvasive glucose concentration as measured using photons optically probing skin.

Skin State Classification

Skin state is optionally classified using a single force pulse or single impulse function, also referred to herein as a ping. Generally, an applied force, such as the force wave 250 provided by the force system 200, takes time to propagate 60 through the subject 320. The travel time of the force wave varies as a function of state of the body, such as hydration, temperature, glucose concentration, triglyceride concentration, hematocrit and/or any constituent of skin, blood, and/or interstitial fluid. Hence, the amount of time to travel radial 65 distances to force wave detectors is optionally used to classify the state of the subject and/or to map the state of the

subject in regions probed by the force wave. For clarity of presentation and without loss of generality, two example of force wave detection are provided here using: (1) a transducer force detector and/or (2) an optical force wave classifier.

Example I

Referring now to FIGS. 10(A-C), transducer force detectors are optionally used to detect transit times of the force wave 250 from the force wave input element 210 to one or more detectors of a set of transducer force detectors 260. Generally, a transducer force detector converts mechanical motion, such as passage of the force wave 250 and/or skin movement into a measured electrical signal. Referring now to FIG. 10A, for clarity of presentation and without loss of generality, a first transducer force detector 262, a second transducer force detector 264, and a third transducer force detector 266 are illustrated that represent n transducer based 20 force detectors, where n is a positive integer of greater than 1, 2, 3, 5, 10, or 20. As illustrated in FIGS. 10B and 10C, the n transducer based force detectors are optionally positioned in a linear array, in a two-dimensional array, and/or along arcs, such as at differing radial distances from one or more light sources in the source system 400. Referring still to FIG. 10A, as illustrated, at a first time, the force wave 250 has propagated to the first transducer force detector 262 as a first wave front position 254; at a second time, t_2 , the force wave 250 has propagated to the second transducer force detector 264 as a second wave front position 256; and at a third time, t_3 , the force wave 250 has propagated to the third transducer force detector 266 as a third wave front position 258. Timing of each wave front to each transducer based force wave detector allows: (1) generation of a sub-surface tissue map of constituents of the skin of the subject 320 using mathematical techniques used for seismic mapping known to those skilled in the art of seismic mapping and/or (2) a classification of state of the subject 320 versus a calibration set of classifying states of force wave propagation radial translation times. For instance, the classification is as simple as slow, medium, or fast translation times to a given transducer detector or a more involved combination of translation times for one or more of: (1) responses at a single detector position and (2) responses at a set of detector positions and/or responses to varying inputs of the force wave, such as time, direction, amplitude, and/or frequency of one or more pings from the force wave input elements and/or time varying induced applied pressure and/or displacement of a portion of the skin of the subject 320 by the force system 200.

Example II

Referring now to FIGS. 11(A-C), propagation of the force wave(s) 250, such as force wave fronts 254, 256, 258 is detected using a set of optical detectors and using the results in a manner similar to detecting the force wave 250 using the set of transducer based wave detectors. For instance, as the force wave 250 propagates through the tissue layers 340, the density, absorbance, and/or scattering of voxels of the skin of the subject 320 change, which alters an observed mean optical path between a given source of photons and a photon/photonic detector. One or more sources of the source system 400 coupled to the array of optical detector elements 510 via the subject 320 is optionally used to detect propagation times of the force wave(s) 250. For clarity of presentation and without loss of generality, a first optical

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detector **521**, a second optical detector **522**, and a third optical detector **523** are illustrated that represent n optical detectors, where n is a positive integer greater than 0, 1, 2, 3, 5, 10, 15, 16, 20, 25, 100, 500, 1000, and 5000. As illustrated in FIGS. **11B** and **11C**, the n optical detectors are optionally positioned in a linear array, in a two-dimensional array, and/or along arcs, such as differing radial distances from one or more light sources in the source system **400** and/or from one or more force wave sources. Notably, one or more detectors of the array of optical detector elements **510** are optionally and preferably used to detect photons from the source system **400** during a measurement phase of an analyte and/or tissue property with or without a tissue classification step. As illustrated, the first optical detector **521** detects a first optical signal, modified by the force wave **250**, with a first pathlength, p_1 , at a given point in time; the second optical detector **522** detects a second optical signal, modified by the force wave **250**, with a second pathlength, p_2 , at the given point in time; and the third optical detector **523** detects a third optical signal, modified by the force wave **250**, with a third pathlength, p_3 , at the given point in time. Each detected optical signal contains absorbances due to any sample constituent, such as water, protein, fat, and/or glucose and/or is representative of state of the tissue, such as a measure of scattering and/or temperature. As the force wave(s) propagate through the tissue, the first, second, and third pathlengths, p_1 , p_2 , p_3 , vary. Hence, the state of the subject **320** is optionally characterized and/or mapped in a manner similar to the transducer wave detection classification and/or mapping; however, optical signals with chemical meaning are used in the process, such as detected intensity, absorbance, and/or scattering related to temperature, one or more tissue layer properties, collagen, elastin, water, albumin, globulin, protein, fat, hematocrit, and/or glucose, such as a concentration, change in tissue state, or a physical structure.

Referring again to FIG. **11A** and FIG. **12A**, the applied pressure/force wave/displacement optionally generates a gap and/or varies an applied pressure at a first interface **305** of the source system **400** and the skin surface **330** and/or at a second interface **390** of the detector system **500** and/or any element thereof and the skin surface **330**. A resulting air gap between the analyzer **110** and the subject **320** and/or a time varying change between an air gap and contact between the analyzer **110** and the subject **320** is used to determine times of contact/relative contact, which is in turn optionally and preferably used in a selection of detected signals step, described infra. For example, loss of optical contact yields a sudden increase in observed intensity in a wavelength region of high absorbance, such as a region dominated by water absorbance in the range of 1350 to 1550 nm, 1400 to 1500 nm, and/or within 5, 10, 15, 25, and/or 50 nm of 1450 nm. Removal of non-contacting signals aids in the development of an outlier analysis algorithm and/or in determining state of the tissue and/or in determination of a degree of applied force from the source system **400**, detector system **500**, and/or analyzer **110** to the skin surface **330** of the subject **320** as a function of time and/or position.

Force Wave/Optical Probe Analyte State Determination

Referring now to FIG. **12**, a process of determining an analyte property, such as a glucose concentration, using one or more optical signals optionally and preferably modified by an applied force, force wave, and/or displacement is provided.

Referring still to FIG. **12**, in a process, such as a first process or a second process, a force is applied **1210**, such as in the form of a force wave and/or displacement induced

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force wave. For example, the force wave/displacement is generated with a transducer to generate application of a transducer force **1212**, which is a single ping **1214**/displacement and/or a series of pings and/or is a force/displacement varied in frequency **1216** and/or varied in amplitude **1218**, such as via a controller, such as a main controller of the analyzer **110**. Subsequently, the force wave **250**/tissue displacement induced pressure propagates in the sample **1220**.

Referring still to FIG. **12**, in another process, such as a first or second process, a result of the tissue displacement induced force wave is measured and/or detected **1230**, such as through a transducer force detection **1232** and/or an optical force detection **1234**.

Referring still to FIG. **12**, in still another process, such as a second and/or third process, selection of a sub-set of detected signals **1240** is performed, such as a function of position **1241**, time **1242**, detector **1243**, contact **1244**, pressure **1245**, and/or spectroscopic response **1246** and an analyte state is determined **1250**, such as via generation of a calibration **1252** and/or use of a generated calibration in a prediction step **1254**.

Multiple-Sensor System

Referring again to FIG. **4A** and referring now to FIG. **13A**, the analyzer **110** optionally comprises multiple sub-sensor systems that operate independently to collect data but operate in concert for determination of state of the subject **320**. For instance the spectrometer **140** optionally comprises a first spectrometer version/system **142** connected/affixed to a first part of the subject **320**, such as on the arm of the subject **320**, and a second spectrometer system/version **144** connected/affixed to a second part of the subject **320**, such as on the leg of the subject **320**. Optionally, the spectrometer **140** is affixed to any part of the body, such as an ear lobe, webbing of the hand, forehead, torso, limb, arm, or leg.

Still referring to FIG. **13A**, generally, the spectrometer **140** refers to n spectrometers/analyzers, where each of the n spectrometers optionally and preferably collects data independently, where n is a positive integer, such as 1, 2, 3, 4, 5, or more. Optionally, each of the n spectrometers collect and analyze data independently. However, preferably, each of the n spectrometers collect data and after little or no pre-processing, collected data is sent to the analyzer **110**, a central processor, a personal communication device, such as a cell phone **122**, and/or to the web for further processing, which allows a central system to process data from the multiple sub-spectrometer systems.

Still referring to FIG. **13A**, optionally, each of the n spectrometers are of the same type and design. However, preferably, each of the n spectrometers are distinct in type and/or design. For instance, the first spectrometer version **142** comprises first sources, optics, and detectors that are directed to measurement of a first constituent/property of the subject **320** and the second spectrometer version **144** comprises second sources, optics, and detectors that are directed to measurement of a second constituent/property of the subject **320**.

Still referring to FIG. **13A**, for example, the n spectrometer systems are optionally and preferably configured to interface to separate portions of the body and/or to measure separate and/or overlapping properties/constituents of the subject **320**, such as percent oxygen saturation, heart rate, heart rate variability, glucose concentration, protein concentration, fat, muscle, protein concentration, albumin concentration, globulin concentration, respiration rate, an electrocardiogram, blood pressure, and/or body temperature and/or environmental temperature and/or acceleration of the subject **320**, such as to indicate a fall of the subject **320** and/or

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an interfering movement of the subject 320 that affects the measurements of the one or more spectrometers 140.

Still referring to FIG. 13A, herein, for clarity of presentation and without loss of generality, the spectrometer 140 is illustrated as a noninvasive glucose concentration analyzer. However, the spectrometer 140 optionally measures any constituent of the body noninvasively, in a minimally invasive manner, and/or operates in conjunction with a noninvasive, minimally invasive, and/or invasive reference system, such as for calibration and quality control procedures. Examples of a first spectrometer version 142 and a second spectrometer version 144 determining an analyte property is provided, infra.

Example I

Referring still to FIG. 13A and referring now to FIG. 13B, an example of interfacing 1300 the analyzer 110 to an arm 370 of the subject 320 is illustrated. As illustrated, a first analyzer/spectrometer version 371 of the analyzer 110 is coupled to a section of an upper arm 372 of the subject's arm and a second analyzer/spectrometer version 373 of the analyzer 110 is coupled to a forearm/wrist 374 of the patient's arm 320. Notably, the first analyzer version 371 interfaces to the subject 320 at a first interface zone along a first z-axis perpendicular to a first x/y-axis plane that is tangential to the subject 320 and that is independent and different from a second interface of the second analyzer version 373, which interfaces to the subject 320 along a second z-axis perpendicular to a second x/y-axis system that is tangential to a second interface zone of the subject. Generally, n analyzers 110, optionally linked to a single main controller 112, interface to n interface zones of the subject 320, where the main controller 112 is optionally and preferably electrically, mechanically, and/or communicatively linked with any and preferably all subsystems of the analyzer 110 and is used to control the analyzer 110, such as via computer hardware and associated software.

Example II

Still referring to FIG. 13B, each of the analyzers interfacing to the subject 320 optionally comprise any system of the analyzer 110. As illustrated, the first analyzer version 371, which is an example of the analyzer 110 comprises three analyzer versions, illustrated as the first spectrometer version 142, the second spectrometer version 144, and the third spectrometer version 146. As illustrated, the first spectrometer version 142, optionally in the form of a watch head, interfaces to the subject 320 along a first z-axis perpendicular to a first x/y-plane, which tangentially touches the upper arm 372 at a first interface point; the second spectrometer version 144 has the form of a watch band link and interfaces to the subject 320 along a second z-axis perpendicular to a second x/y-plane, which tangentially touches the upper arm 372 at a second interface point; and the third spectrometer version 146, optionally in the form of a watch band attachment, interfaces to the subject 320 along a third z-axis perpendicular to a third x/y-plane, which tangentially touches the upper arm 372 at a third interface point. Each of the three spectrometer versions 142, 144, 146 are optionally attached to the upper arm 146 via double-sided adhesives and are thus attached in the manner of a sticker. As illustrated, the three spectrometer versions 142, 144, 146 are attached to the upper arm 372 with a flexible band 148, such as a watch band or an elastic band. The individual spectrometer versions 142, 144, 146 are option-

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ally connected using one or more hinge components and or rotating connectors. The individual spectrometer versions 142, 144, 146 are optionally replaceably connected to the subject along separate planes forming angles therebetween of greater than 1, 2, 5, 10, 15, 25, or 25 degrees. The hinge allows tangential interfacing of illumination zones of the respective spectrometer version along a curved surface of the subject 320. Optionally, the hinge allows for rotation of a first spectrometer unit relative to a second spectrometer unit to maintain tangential contact of the illumination zones with the subject 320 as the skin of the subject moves, such as by allowing a rotation of greater than 0.1, 0.5, 1, 2, or 5 degrees. The multiple planes of attachment of the analyzer 110 to the subject 320 allow attachment of multiple sources and/or detectors to the subject 320 along a curved skin surface of the subject 320, such as around the upper arm 372 and/or the lower arm 374, as illustrated with the second analyzer/spectrometer version 373 attached to the wrist of the subject 320, with minimal applied tissue deformation forces at each of the analyzer/subject interface zones. Reduced forces, such as an applied mass, stress, and/or strain aids precision and/or accuracy of the analyzer 110 by reducing movement of fluids within the tissue layers 340 of the subject 320, reducing changes in pathlength, and/or reducing changes in pressure induced scattering of light.

Example III

Still referring to FIG. 13B, in a first case, each of the first spectrometer version 142, second spectrometer version 144, and third spectrometer version 146 optionally contain all of the functionality of the analyzer 110. However, optionally, one or more optical sources are in one interfacing aspect of the first analyzer version 371, such as in the second spectrometer version 144, without any functional optical detectors in the second spectrometer version 144. In this case, the optical detectors are in a second interfacing aspect of the first analyzer version 371, such as in the first spectrometer version 142. For clarity of presentation and without loss of generality, a particular example is provided. In this example, the detector system 500 is positioned in the analyzer 110 in the first spectrometer version 142 along with optional illuminators of the source system 400. However, the source system also includes photon sources in the second spectrometer version 144, such as in a watch band link position. In this manner, photonic illuminators with short optical distances to the detector system 500 are positioned in the first spectrometer version 142, such as in close proximity to the detector system 500. For instance, photonic sources emitting in wavelength ranges: (1) with an optical absorbance of greater than one unit per millimeter of pathlength and/or (2) in the 1350 to 1560 nm range, such as within 25 mm of 1510, 1520, 1530, or 1540 nm are positioned near the detector system 500, such as in the same housing as the detector system 500, in the first spectrometer version 142, and/or with a radial distance between an illumination zone and a detection zone of less than 10, 8, 6, 5, 4, 3, 2, 1.5, or 1 millimeters. However, photonic sources emitting in lower absorbance regions, such as from 400 to 1350 nm and/or 1565 to 1800 and/or in regions of absorbance by skin at a level of less than one absorbance unit per millimeter of pathlength are positioned in the second spectrometer version 144, thus giving the photons a longer pathlength to the detector system 500 in the first spectrometer version 142. The longer selected pathlength, as selected by a detector element of the detector system 500, from a given source reduces a range of observed pathlengths by photons from the

given source, as described supra. Further, each spectrometer version **142**, **144**, **146** allows an independent mean photon path entering the skin of the subject **320** to be perpendicular to the subject **320** despite the radius of curvature of the skin of the subject **320** as the differing spectrometer versions **142**, **144**, **146** are each positioned with an x/y-plane interface tangential to the local curvature of the skin of the subject **320**, such as at different positions on a watch band equivalent. Optionally and preferably, the x/y-planes tangential to the subject **320** at local sample interface sites for the n interface points of the analyzer **110**, such as the first interface location of the first spectrometer version **142**, the second interface location of the second spectrometer version **144**, and the third interface location of the third spectrometer version **146** are separated by greater than 5, 6, 7, 8, 9, 10, 12, 14, 16, 18, or 20 millimeters as measured along the skin surface. Hence, second photon sources for providing second wavelengths for measuring oxygen and/or scattering of light, such as from 400 to 1300 nm, are optionally placed in a second housing along a second position of the watch band while first photon sources for providing first wavelengths, such as at glucose absorbing wavelengths from 1500 to 2400 nm, are optionally placed in a first housing proximate detector elements, where the detector elements in the first housing detect photons from second, third, . . . , nth housings, such as along a circumferential band around a curved body part, where n is a positive integer greater than 1, 2, or 3.

Example IV

In the first spectrometer version **371** of the analyzer **110**, three sample interface zones are used, a first sample interface zone, such as the back of a watch zone where the source system **400**, force system **200**, and/or a first set of optics, such as in the first spectrometer version **142**, interface to the subject **320**; a second interface zone, such as where a second set of optics, such as in the second spectrometer version **144**, interface to the subject **320**; and a third interface zone, such as where a third set of optics, such as in a third spectrometer version **146**, interface to the subject **320**. Generally, any number n of sets of optics interface to the subject **320** to yield n sets of data on a state of the subject **320** where n is a positive integer, such as 1, 2, 3, 4, 5 or more. Optionally, the n sets of optics generate simultaneous data on a single state of the subject **320**. However, each sub-set of optics in the n sets of optics are optionally configured to measure the same analyte and/or different analytes, such as one of more of percent oxygen saturation, heart rate, heart rate variability, glucose concentration, protein concentration, fat, muscle, protein concentration, albumin concentration, globulin concentration, respiration rate, an electrocardiogram, blood pressure, body temperature, environmental temperature, and acceleration of the subject **320**.

Depth Resolution

Photons scatter in tissue. However, a mean photon path between an illumination zone and a detection zone has a mean/medium/average depth of penetration into the skin layers **340** and glucose is present at differing concentrations as a function of depth into the skin layers **340**. A target zone of probing photons is the epidermis **344** and/or dermis **346** between the stratum corneum **342** and the subcutaneous fat **348**. Targeting these well perfused tissue layers is described herein by way of non-limiting examples.

Example I

Referring now to FIG. **14A**, an example of a probe tip **1400** of the source system **400** of the analyzer **110** is

presented. The probe tip has a tissue contacting surface **1410** and at least one illumination zone **1420**. For clarity of presentation and without loss of generality, a single illumination zone is illustrated which is optionally and preferably one illumination zone of a plurality of illumination zones, such as where a given illumination zone is a surface area of the skin/probe tip interface illuminated by a given source, such as a given light emitting diode. More particularly, 2, 3, 4, or 5, or more, light emitting diodes/laser diodes couple to the skin, optionally via intervening optics of the photon transport system **450**, to illuminate a corresponding second, third, fourth, and fifth, or more, skin/probe tip interface areas, referred to herein as illumination zones. Similarly, a given detector element optically couples, such as by the photon transport system **450** to a given surface area of the skin/probe tip interface, which is referred to as a detection zone. More particularly, 2, 3, 4, or 5, or more, detector elements, of the detector system **500**, optically interface, such as through optics of the photon transport system **450** with the skin, to detect photons emitting from a corresponding second, third, fourth, and fifth, or more, skin/probe tip interface area, referred to herein as detection zones. A mean optical path for a set of photons is a mean pathway through the tissue layers **340** of the subject **320** between a given illumination zone and a given detection zone. Optionally, the probe tip **1400** is of any geometry. Optionally, illumination zones are of any pattern on the probe tip **1400**. Optionally, detection zones are of any layout on the probe tip **1400**.

Example II

Referring still to FIG. **14A** and referring now to FIG. **14B**, resolution of a mean depth of penetration of probing photons between an illumination zone and rings of detectors **1430** is provided. As illustrated, a first ring of detectors **1432**, coupled to a first set of detection zones, is at a first radius, r_1 , from the illumination zone and a second set of detectors **1434**, coupled to a second set of detection zones, is at a second radius, r_2 , from the illumination zone. For clarity of presentation and without loss of generality, the detectors and detector zones are illustrated with the same circular graphical representation herein. Further, the circular graphical representations are optionally illustrative of the ends of fiber optics coupled to corresponding detectors or sources. At close distances having an observed absorbance of less than one, the mean depth of penetration of probing photons increases with radial distance. The first and second ring of detectors **1432**, **1434** are separated by a radial distance difference, Δr_1 . Referring now to FIG. **14B**, the first ring of detectors **1432** corresponds to a first mean optical path **1472** having a first depth of penetration into the tissue layers **340** and the second ring of detectors **1434** corresponds to a second mean optical path **1474** having a second depth of penetration into the tissue layers **340**. As illustrated, for a first radial detector **1482** at the first radial distance, r_1 , the maximum depth of the first mean optical path **1472** and the second mean optical path, for a second radial detector **1484** at a second radial distance, r_2 , have a depth of penetration difference, Δd_1 . Notably, the second ring of detectors **1434** is spatially positioned at a closest linear distance, the line passing through the illumination zone **1420**, to the first ring of detectors **1432**. Thus, the best resolution of depth is the depth of penetration difference, Δd_1 , corresponding to a first range of tissue thicknesses **1482**. However, in many cases, as the thicknesses of the epidermis **344** and dermis **346** changes with applied pressure, force, hydration, spatial orientation, movement, and/or changes in blood constituent

concentration, the targeted dermal layers are not resolved using the best resolution of concentric detector rings with a difference in radial distance, Δr_1 , to the illumination zone **1420** corresponding to the resolved depth, Δd_1 .

Example III

Referring still to FIG. **14A** and FIG. **14B** and referring now to FIG. **14C**, a comparison of resolution of a mean depth of penetration of probing photons between an illumination zone and rings of detectors **1430** and arcs of detectors **1450** is provided. Herein, an arc of detectors is a set of detectors along a curved path of multiple radial distances from an illumination zone. The arced path is not an arc of a circle. Rather, the arced path is along a spiral and/or curve covering a range of radial distances from an illumination zone. As illustrated an arc of detectors **1450**, along an optional arc layout **1462**, starts at the first radial distance, r_1 , of the first ring of detectors **1432** and ends at the second radial distance, r_2 , of the second ring of detectors. While the first and second ring of detectors have a first linear radial distance difference, r_1 , that is based on the size of the detector element housing, fiber optic, and/or detection zone, the illustrated arc of detectors **1450** has a second linear radial distance difference, r_2 , that is smaller than, r_1 . Particularly, with the seven illustrated detectors in the arc of detectors, the second linear radial distance, r_2 , is one-seventh that of the first radial distance, r_1 . Generally, the difference in radial distance is better than $1/2$, $1/3$, $1/4$, $1/5$, . . . , $1/n$ that of the spatially constrained concentric rings of detectors for n detector elements in an arc bounded by the first and second radial distances, r_1 and r_2 , of the concentric rings of detectors, where n is a positive integer of greater than 2, 3, 4, 5, 10, or 20. Comparing now the first and second mean depths of penetrations **1472**, **1474** for the first and second ring of detectors **1432**, **1434** and the first and second detector **1482**, **1484**, with the range of mean depths of penetrations in FIG. **14C** corresponding to the individual illumination zone **1420** to detection zones of detector elements in the ring of detector elements **1450**, the enhanced resolution is illustratively obvious. Particularly, the above described first resolved depth, Δd_1 , corresponding to the first and second ring of detectors **1432**, **1434** is seven times larger than a second resolved depth, Δd_2 , between a third mean path **1437** and a fourth mean path **1474** corresponding to the second radial detector **1484** and a closest intermediate radial detector **1486**, two detector elements in the arc of detectors **1450**. Particularly, a second range of tissue thicknesses **1484** is thinner than the first range of tissue thicknesses **1482**, described supra. Generally, the difference in resolved tissue depth is better than $1/2$, $1/3$, $1/4$, $1/5$, . . . , $1/n$ that of the spatially constrained concentric rings of detectors for n detector elements in an arc bounded by the first and second radial distances, r_1 and r_2 , of the concentric rings of detectors, where n is a positive integer of greater than 2, 3, 4, 5, 10, or 20. Thus, arcs of detection zones corresponding to arcs of detectors and/or coupling optics, such as fiber optics, spanning a range of radial distances from an illumination zone yield an enhanced resolution of tissue depth. Further, as described supra, dynamic selection of signals from detector elements radially inward from an outwardly positioned detector element observing a disproportionate increase in a fat band absorbance, which is an example of a spectroscopic marker, from the subcutaneous fat **348**, at a greater depth than the targeted dermis **346**, yields the largest radial distance observing the desired/targeted dermal layers. Further, as the epidermis **344** and dermis **346** change in thickness,

such as due to subject movement, orientation, and/or hydration, and/or changes in body chemistry, the range of resolved depths of penetration corresponding to the range of radial distances between the illumination zone and individual detection zones allows dynamic selection of source-to-detector distances currently probing the desired dermal layers, such as the epidermis **344** and the dermis **346**.

Acousto-Optic Analyzer Vs. (1) UPI and (2) an AOTF

An applied force-optic analyzer is described herein. Optionally and preferably, the applied force results in a mechanical disturbance of the tissue resulting in a force being applied to the sample. However, in a sub-case of the applied force-optic analyzer, the applied force comprises an acoustic force yielding an acousto-optic analyzer. Notably, in the sub-case of the applied force-optic analyzer being an acousto-optic analyzer, as used herein an acousto-optic analyzer starkly contrasts with both: (1) an ultrasonic photoacoustic imaging (UPI) system and (2) an acousto-optic tunable filter (AOTF) spectrometer, as described infra.

Acousto-Optic Analyzer

As described, an acousto-optic analyzer (AOA) introduces an acoustic vibration wave to the sample to impact the state of the sample, such as tissue, and the state of the sample is measured using an optical probe.

Photoacoustic Imaging

In stark contrast, according to Wikipedia, ultrasonic photoacoustic imaging, also referred to as (UPI), photoacoustic imaging (PI), and/or optoacoustic imaging, delivers non-ionizing laser pulses to biological tissue, which results in absorbed energy and resultant heat in the form of transient thermoelastic expansions detected as wideband megaHertz ultrasonic emissions detected by ultrasonic transducers. The detected signals are used to produce images. As optical absorbance relationships exist with physiological properties, such as hemoglobin concentration and oxygen saturation, the detected pressure waves may be used to determine hemoglobin and oxygen concentration.

Hence, an acousto-optic analyzer starkly contrasts with photoacoustic imaging. Stated again, while the acousto-optic analyzer described herein may induce a heat wave like in photoacoustic imaging, in photoacoustic imaging the sound wave is detected whereas photons, from an external source, are detected in the acousto-optic analyzer described are detected after interacting with the sample being displaced/heated/disturbed by the sound wave.

Acousto-Optic Tunable Filter

According to Wikipedia, an acousto-optic tunable filter (AOTF), diffracts light based on an acoustic frequency. By tuning the frequency of the acoustic wave, the desired wavelength of the optical wave can be diffracted acousto-optically.

Hence, an acousto-optic analyzer (AOA) starkly contrasts with an acousto-optic tunable filter (AOTF) as, while the input sound wave of the AOA may diffract light, the separation of the input light is not the primary use of the sound wave. Indeed, a narrow-band light emitting diode (LED) is optionally used in conjunction with a broadband detector in the acousto-optic analyzer making any separation of the narrow band light source pointless. Further, in the AOA, the sound wave is used to change the state of the biological sample itself, whereas in the AOTF the sound wave is introduced to a birefringent crystal in a wavelength separation module of the spectrometer and is not introduced into the sample.

Still yet another embodiment includes any combination and/or permutation of any of the elements described herein.

The main controller, a localized communication apparatus, and/or a system for communication of information optionally comprises one or more subsystems stored on a client. The client is a computing platform configured to act as a client device or other computing device, such as a computer, personal computer, a digital media device, and/or a personal digital assistant. The client comprises a processor that is optionally coupled to one or more internal or external input device, such as a mouse, a keyboard, a display device, a voice recognition system, a motion recognition system, or the like. The processor is also communicatively coupled to an output device, such as a display screen or data link to display or send data and/or processed information, respectively. In one embodiment, the communication apparatus is the processor. In another embodiment, the communication apparatus is a set of instructions stored in memory that is carried out by the processor.

The client includes a computer-readable storage medium, such as memory. The memory includes, but is not limited to, an electronic, optical, magnetic, or another storage or transmission data storage medium capable of coupling to a processor, such as a processor in communication with a touch-sensitive input device linked to computer-readable instructions. Other examples of suitable media include, for example, a flash drive, a CD-ROM, read only memory (ROM), random access memory (RAM), an application-specific integrated circuit (ASIC), a DVD, magnetic disk, an optical disk, and/or a memory chip. The processor executes a set of computer-executable program code instructions stored in the memory. The instructions may comprise code from any computer-programming language, including, for example, C originally of Bell Laboratories, C++, C#, Visual Basic® (Microsoft, Redmond, Wash.), Matlab® (MathWorks, Natick, Mass.), Java® (Oracle Corporation, Redwood City, Calif.), and JavaScript® (Oracle Corporation, Redwood City, Calif.).

Herein, any number, such as 1, 2, 3, 4, 5, is optionally more than the number, less than the number, or within 1, 2, 5, 10, 20, or 50 percent of the number.

Herein, an element and/or object is optionally manually and/or mechanically moved, such as along a guiding element, with a motor, and/or under control of the main controller.

The particular implementations shown and described are illustrative of the invention and its best mode and are not intended to otherwise limit the scope of the present invention in any way. Indeed, for the sake of brevity, conventional manufacturing, connection, preparation, and other functional aspects of the system may not be described in detail. Furthermore, the connecting lines shown in the various figures are intended to represent exemplary functional relationships and/or physical couplings between the various elements. Many alternative or additional functional relationships or physical connections may be present in a practical system.

In the foregoing description, the invention has been described with reference to specific exemplary embodiments; however, it will be appreciated that various modifications and changes may be made without departing from the scope of the present invention as set forth herein. The description and figures are to be regarded in an illustrative manner, rather than a restrictive one and all such modifications are intended to be included within the scope of the present invention.

Accordingly, the scope of the invention should be determined by the generic embodiments described herein and their legal equivalents rather than by merely the specific examples described above. For example, the steps recited in any method or process embodiment may be executed in any order and are not limited to the explicit order presented in the specific examples. Additionally, the components and/or elements recited in any apparatus embodiment may be assembled or otherwise operationally configured in a variety of permutations to produce substantially the same result as the present invention and are accordingly not limited to the specific configuration recited in the specific examples.

Benefits, other advantages and solutions to problems have been described above with regard to particular embodiments; however, any benefit, advantage, solution to problems or any element that may cause any particular benefit, advantage or solution to occur or to become more pronounced are not to be construed as critical, required or essential features or components.

As used herein, the terms “comprises”, “comprising”, or any variation thereof, are intended to reference a non-exclusive inclusion, such that a process, method, article, composition or apparatus that comprises a list of elements does not include only those elements recited, but may also include other elements not expressly listed or inherent to such process, method, article, composition or apparatus. Other combinations and/or modifications of the above-described structures, arrangements, applications, proportions, elements, materials or components used in the practice of the present invention, in addition to those not specifically recited, may be varied or otherwise particularly adapted to specific environments, manufacturing specifications, design parameters or other operating requirements without departing from the general principles of the same.

Although the invention has been described herein with reference to certain preferred embodiments, one skilled in the art will readily appreciate that other applications may be substituted for those set forth herein without departing from the spirit and scope of the present invention. Accordingly, the invention should only be limited by the Claims included below.

The invention claimed is:

1. A method for noninvasively determining a sample constituent property of a person having skin, comprising the steps of:

providing an analyzer comprising a main controller, said main controller:

controlling photon generation from at least a first source of a set of optical sources and analyzing signal from a set of detectors;

at a first time, irradiating an illumination zone of the skin with a current set of photons from said first source;

detecting a portion of the current set of photons, after passage through the skin of the person, with each detector of said set of detectors, said set of detectors respectively optically coupled to a set of detection zones of the skin positioned along a spiral path from a first radial distance from the illumination zone to a second radial distance from the illumination zone, wherein a first detection zone of a first detector of said set of detectors extends radially outward from said

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illumination zone to at least an inward radial distance of a second detector of said set of detectors, wherein at least one detection zone of said set of detection zones has a central radial distance from said illumination zone between the first radial distance and the second radial distance; and

resolving a dermal depth of the skin of the patient from a subcutaneous fat depth via differences between responses of said set of detectors coupled to said spiral path,

said main controller selecting current signals from a first subset of said set of detectors for determination of said sample constituent property.

2. The method of claim **1**, further comprising the step of: at a second time, the current set of photons comprising second photons originating from a second source of said set of sources, the first photons transmitting into the skin of the person along a first line, the second set of photons transmitting into the skin of the person along a second line, the first line and the second line forming an angle greater than fifteen degrees.

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3. The method of claim **2**, further comprising the step of: using an adhesive layer to mount said first source and the second source to the skin of the person at the angle therebetween of greater than fifteen degrees.

4. The method of claim **1**, further comprising the steps of: affixing a skin displacement inducing electro-mechanical transducer, of said analyzer, to the skin of the subject; and

said main controller driving the skin displacement through application of a waveform driving signal to said electro-mechanical transducer.

5. The method of claim **4**, further comprising the step of: said step of detecting functioning during displacement of the skin by said electro-mechanical transducer.

6. The method of claim **5**, said step of selecting comprising the step of: time-correlating responses from said set of detectors with said waveform driving signal.

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